# Standard for the Installation of Centrifugal Fire Pumps 1996 Edition



### NOTICE

All questions or other communications relating to this document should be sent only to NFPA headquarters, addressed to the attention of the Committee responsible for the document.

For information on the procedures for requesting Technical Committees to issue Formal Interpretations, proposing Tentative Interim Amendments, proposing amendments for Committee consideration, and appeals on matters relating to the content of the document, write to the Secretary, Standards Council, National Fire Protection Association, 1 Batterymarch Park, P.O. Box 9101, Quincy, MA 02269-9101.

A statement, written or oral, that is not processed in accordance with Section 5 of the Regulations Governing Committee Projects shall not be considered the official position of NFPA or any of its Committees and shall not be considered to be, nor be relied upon as, a Formal Interpretation.

Users of this document should consult applicable federal, state and local laws and regulations. NFPA does not, by the publication of this document, intend to urge action that is not in compliance with applicable laws, and this document may not be construed as doing so.

### Policy Adopted by NFPA Board of Directors on December 3, 1982

The Board of Directors reaffirms that the National Fire Protection Association recognizes that the toxicity of the products of combustion is an important factor in the loss of life from fire. NFPA has dealt with that subject in its technical committee documents for many years.

There is a concern that the growing use of synthetic materials may produce more or additional toxic products of combustion in a fire environment. The Board has, therefore, asked all NFPA technical committees to review the documents for which they are responsible to be sure that the documents respond to this current concern. To assist the committees in meeting this request, the Board has appointed an advisory committee to provide specific guidance to the technical committees on questions relating to assessing the hazards of the products of combustion.

Licensing Provision—This document is copyrighted by the National Fire Protection Association (NFPA).

- 1. Adoption by Reference—Public authorities and others are urged to reference this document in laws, ordinances, regulations, administrative orders, or similar instruments. Any deletions, additions, and changes desired by the adopting authority must be noted separately. Those using this method are requested to notify the NFPA (Attention: Secretary, Standards Council) in writing of such use. The term "adoption by reference" means the citing of title and publishing information only.
- 2. Adoption by Transcription—A. Public authorities with lawmaking or rule-making powers only, upon written notice to the NFPA (Attention: Secretary, Standards Council), will be granted a royalty-free license to print and republish this document in whole or in part, with changes and additions, if any, noted separately, in laws, ordinances, regulations, administrative orders, or similar instruments having the force of law, provided that: (I) due notice of NFPA's copyright is contained in each law and in each copy thereof; and (2) that such printing and republication is limited to numbers sufficient to satisfy the jurisdiction's lawmaking or rule-making process. B. Once this NFPA Code or Standard has been adopted into law, all printings of this document by public authorities with lawmaking or rule-making powers or any other persons desiring to reproduce this document or its contents as adopted by the jurisdiction in whole or in part, in any form, upon written request to NFPA (Attention: Secretary, Standards Council), will be granted a nonexclusive license to print, republish, and vend this document in whole or in part, with changes and additions, if any, noted separately, provided that due notice of NFPA's copyright is contained in each copy. Such license shall be granted only upon agreement to pay NFPA a royalty. This royalty is required to provide funds for the research and development necessary to continue the work of NFPA and its volunteers in continually updating and revising NFPA standards. Under certain circumstances, public authorities with lawmaking or rule-making powers may apply for and may receive a special royalty where the public interest will be served thereby.
- 3. Scope of License Grant—The terms and conditions set forth above do not extend to the index to this document.

(For further explanation, see the Policy Concerning the Adoption, Printing, and Publication of NFPA Documents, which is available upon request from the NFPA.)

### Statement on NFPA Procedures

This material has been developed under the published procedures of the National Fire Protection Association, which are designed to assure the appointment of technically competent Committees having balanced representation. While these procedures assure the highest degree of care, neither the National Fire Protection Association, its members, nor those participating in its activities accept any liability resulting from compliance or noncompliance with the provisions given herein, for any restrictions imposed on materials or processes, or for the completeness of the text.

NFPA has no power or authority to police or enforce compliance with the contents of this document, and any certification of products stating compliance with requirements of this document is made at the peril of the certifier.

### Errata

# **NFPA 20**

# **Installation of Centrifugal Fire Pumps**

### 1996 Edition

Reference: 7-9.1 and 9-5.2.1(c) (New)

The Technical Committee on Fire Pumps notes the following errors in the 1996 edition of NFPA 20, Standard for the Installation of Centrifugal Fire Pumps.

- 1. In 7-9.1, after the phrase "Sections 7-1 through 7-5", add the words "or 7-7".
- 2. In 9-5.2.1, add the following text:
  - (c) There shall be no shutoff valve in the pressure sensing line.

Issue Date: October 23, 1996

Copyright © 1996 All Rights Reserved NATIONAL FIRE PROTECTION ASSOCIATION

CHARLES S. MORGAN LIBRARY
NATIONAL FIRE PROTECTION ASSOCIATION
1 BATTERYMARCH PARK
QUINCY, MA 02269-9101

# CHARLES S. MORGAN LIBRARY NATIONAL FIRE PROTECTION ASSOCIATION 1 BATTERYMARCH PARK

QUINCY, MA 02269-9101 Copyright © 1996 NFPA, All Rights Reserved

### NFPA 20

### Standard for the Installation of

### Centrifugal Fire Pumps

### 1996 Edition

This edition of NFPA 20, Standard for the Installation of Centrifugal Fire Pumps, was prepared by the Technical Committee on Fire Pumps and acted on by the National Fire Protection Association, Inc., at its Annual Meeting held May 20–23, 1996, in Boston, MA. It was issued by the Standards Council on July 18, 1996, with an effective date of August 9, 1996, and supersedes all previous editions.

Changes other than editorial are indicated by a vertical rule in the margin of the pages on which they appear. These lines are included as an aid to the user in identifying changes from the previous edition.

This document has been submitted to ANSI for approval.

### Origin and Development of NFPA 20

The first National Fire Protection Association standard for automatic sprinklers was published in 1896 and contained paragraphs on steam and rotary fire pumps.

The Committee on Fire Pumps was organized in 1899 with five members from underwriter associations. Today the committee membership includes representatives of Underwriters' Laboratories of both the United States and Canada, Insurance Services Offices, Factory Mutual, Industrial Risk Insurers, national trade associations, state government, engineering organizations, and private individuals.

Early fire pumps were only secondary supplies for sprinklers, standpipes, and hydrants, and were started manually. Today, fire pumps have greatly increased in number and in applications: many are the major or only water supply, and almost all are started automatically. Early pumps usually took suction by lift from standing or flowing water supplies because the famed National Standard Steam Fire Pump and rotary types suited that service. Ascendancy of the centrifugal pump resulted in positive head supply to horizontal shaft pumps from public water supplies and aboveground tanks. Later, vertical shaft turbine-type pumps were lowered into wells or into wet pits supplied from ponds or other belowground sources of water.

Gasoline-engine-driven pumps first appeared in this standard in 1913. From an early status of relative unreliability and of supplementary use only, first spark-ignited gasoline engines and then compression ignition diesels have steadily developed engine-driven pumps to a place alongside electric-driven units for total reliability.

Fire protection now calls for larger pumps, higher pressures, and more varied units for a wide range of systems protecting both life and property. Hydraulically calculated and designed sprinkler and special fire protection systems have changed concepts of water supply completely.

Since the formation of this Committee, each edition of NFPA 20 has incorporated appropriate provisions to cover new developments and has omitted obsolete provisions. NFPA action on successive editions has been taken in the following years: 1907, 1910–13, 1915, 1918–21, 1923–29, 1931–33, 1937, 1939, 1943, 1944, 1946–48, 1951, 1953, 1955, 1957, 1959–72, 1974, 1976, 1978, 1980, 1983, and 1987.

The 1990 edition included several amendments with regard to some of the key components associated with electric-driven fire pumps. In addition, amendments were made to allow the document to conform more closely to the NFPA Manual of Style.

The 1993 edition included significant revisions to Chapters 6 and 7 with regard to the arrangement of the power supply to electric-driven fire pumps. These clarifications were intended to provide the necessary requirements in order to make the system as reliable as possible.

The 1996 edition of the standard continues the changes initiated in the 1993 edition as Chapters 6 and 7, which address electric drives and controllers, underwent significant revision. New information was also added regarding engine cooling provisions, earth-quake protection, and backflow preventors. Chapter 5, which addressed provisions for high-rise buildings, was removed, as were capacity limitations on in-line and end-suction pumps. Additionally, provisions regarding suction pipe fittings were updated.

### **Technical Committee on Fire Pumps**

Thomas W. Jaeger, Chair Gage Babcock & Assoc., Inc., VA

Kerry M. Bell, Underwriters Laboratories Inc., IL

John R. Bell, Westinghouse Hanford Co., WA Harold D. Brandes, Jr., Duke Power Co., NC

Rep. Electric Light Power Group/Edison Electric Inst.

Walter A. Damon, Schirmer Engr Corp., IL

Manuel J. DeLerno, S-P-D Industries Inc., IL

Rep. Illinois Fire Prevention Assn.

David Dixon, Security Fire Protection, TN

Rep. Nat'l Fire Sprinkler Assn.

Donald K. Dorini, Gulfstream Pump & Equipment Co., FL

George W. Flach, Flach Consultants, LA

Randall Jarrett, Patterson Pump Co., GA

Rep. Hydraulic Inst.

John D. Jensen, Protection Consultants Inc., ID

Donald L. Johnson, Kemper Nat'l Insurance Cos., IL

James D. Kahlenbeck, Cummins Engine Co., IN

Rep. Engine Mfrs. Assn.

Antonio C. M. Braga, Factory Mutual Research Corp., MA (Alt. to W. E. Wilcox)

Salvatore A. Chines, Industrial Risk Insurers, CT

(Alt. to E. D. Leedy)

Phillip A. Davis, Kemper Nat'l Insurance Cos., PA (Alt. to D. L. Johnson)

David A. de Vries, Schirmer Engr Corp., IL

(Alt. to W. A. Damon)

Alan A. Dorini, Gulfstream Pump & Equipment Co., FL (Alt. to D. K. Dorini)

Dennis N. Gage, ISO Commercial Risk Services, Inc., NJ (Alt. to M. Marvi)

Donald Hansen, Aurora Pump, IL

(Alt. to R. Jarret)

Kenneth E. Isman, Nat'l Fire Sprinkler Assn., NY

(Alt. to D. Dixon)

Cléement Leclerc, Armstrong Darling Inc., PQ, Canada

Edward D. Leedy, Industrial Risk Insurers, IL

Rep. Industrial Risk Insurers

R. T. Leicht, CIGNA Loss Control Services Inc., DE Rep. American Insurance Services Group, Inc.

Maurice Marvi, ISO Commercial Risk Services, Inc., NJ Bernard McNamee, Underwriters Laboratories of Canada,

ON, Canada

R. W. Montembeault, Peerless Pump Co., IN

David S. Mowrer, HSB Professional Loss Control, Inc., TN

Richard Schneider, Joslyn Clark Controls, SC

Rep. Nat'l Electrical Mfrs. Assn.

Jay A. Stewart, Jay Stewart Assn. Inc., MI

Rep. Chemical Mfrs. Assn.

Lee Ulm, ITT Corp., OH

William E. Wilcox, Factory Mutual Research Corp., MA

### Alternates

Timothy S. Killion, Peerless Pump Co., IN

(Alt. to R. W. Montembeault)

John R. Kovacik, Underwriters Laboratories Inc., IL

(Alt. to K. M. Bell)

Terence A. Manning, Manning Electrical Systems, Inc., IL

(Alt. to M. J. DeLerno)

William N. Matthews, Jr., Duke Power Co., NC

(Alt. to H. D. Brandes, Jr.)

Thomas J. O'Brien, Gage Babcock & Assoc., Inc., IL

(Alt. to T. W. Jaeger)

Jeffrey L. Robinson, Westinghouse Savannah River Co., SC

(Alt. to J. R. Bell)

William F. Stelter, Master Control Systems, Inc., IL

(Alt. to R. Schneider)

Bruce Wilber, CIGNA Property and Casualty Co., CA

(Alt. to R. T. Leicht)

### Nonvoting

James W. Nolan, James W. Nolan Co., IL (Member Emeritus)

### Milosh T. Puchovsky/Robert Solomon, NFPA Staff Liaisons

This list represents the membership at the time the Committee was balloted on the text of this edition. Since that time, changes in the membership may have occurred.

NOTE: Membership on a Committee shall not in and of itself constitute an endorsement of the Association or any document developed by the Committee on which the member serves.

Committee Scope: This Committee shall have primary responsibility for documents on the selection and installation of stationary pumps supplying water or special additives including but not limited to foam concentrates for private fire protection, including suction piping, valves and auxiliary equipment, electric drive and control equipment, and internal combustion engine drive and control equipment.

### NOTICE

Following the issuance of this edition of NFPA 20, Standard for the Installation of Centrifugal Fre Pumps, by the NFPA Standards Council, an appeal was filed with the NFPA Board of Directors.

The appeal requests that the Board of Directors reverse the Standards Council decision and issue the 1996 edition of NFPA 20 with the second and third sentences of 3-1.1 as contained in the previous (1993) edition. These provisions provided capacity limitations for certain types of in-line and end-suction fire pumps.

NFPA will announce the disposition of the appeal when it has been determined. Anyone wishing to receive the disposition of the appeal should notify in writing the Secretary, Standards Council, NFPA, 1 Batterymarch Park, P.O. Box 9101, Quincy, MA 02269-9101.

**20-**3

### **Contents**

Chapter	1 Introduction 20- 4	6-3 Power Supply Lines 20-16
1-1	Scope	
1-2	Purpose	
1-3	Other Pumps	
1-4	Approval Required 20-4	1
1-5	Pump Operation 20- 4	Chapter 7 Electric Drive Controllers and
1-6	Unit Performance 20- 4	Accessories
1-7	Certified Shop Test 20- 4	4 7-1 Application
1-8	Definitions	1-2 Location
1-9	Units	
<b>.</b>		7-4 Components
	2 General	
2-1	Water Supplies	
2-2	Pumps and Drivers 20-	
2-3	Rated Pump Capacities 20-	
2-4	Nameplate	
2-5	Pressure Gauges	
2-6	Circulation Relief Valve 20-	
2-7	Equipment Protection 20-	Chapter of Dieser Emplife Drive
2-8	Pipe and Fittings 20- 8	8-1 General 20_99
2-9	Suction Pipe and Fittings 20-8	8-2 Engines
2-10	Discharge Pipe and Fittings 20- 9	8-3 Pump and Engine Protection 20-26
2-11	Valve Supervision 20- 9	8-4 Fuel Supply and Arrangement 20-26
2-12	Protection of Piping Against Damage Due to	8-5 Engine Exhaust 20-26
	Movement	8-6 Driver System Operation
2-13	Relief Valve	,
2-14	Waterflow Test Devices 20-10	
2-15	Power Supply Dependability 20–10	
2-16	Shop Tests	
2-17	Pump Shaft Rotation 20-10	
2-18	Alarms	
2-19	Pressure Maintenance (Jockey or Make-Up)	• 9-5 Starting and Control 20–28
	Pumps	9-6 Air Starting Engine Controllers 20-30
2-20	Summary of Fire Pump Data 20-11	Chapter 10 Steam Turbine Drive 20-31
2-21	Backflow Preventers and Check Valves 20-11	10-1 General
2-22	Earthquake Protection 20–11	10-2 Turbine
Chanter	3 Horizontal and In-Line Pumps 20-11	100 7 11 1
3-1	General	
3-1 3-2	Factory and Field Performance 20–12	,,,,,,,,,
3-2 3-3	Fittings	
3-3 3-4		11 1 11/4:00:4::0 10::0 4::4::1:4::1:5::1:5::1:5::1:5::1:5::1:5
	Foundation and Setting 20-12	
3-5	Connection to Driver and Alignment 20–12	
Chapter -	4 Vertical Shaft Turbine-Type Pumps 20-12	Parts
4-1	General	11-4 Periodic Inspection, Testing, and
4-2	Water Supply	Maintenance
4-3	Pump	
4-4	Installation	
4-5	Driver	
4-6	Tests	
4-7	Operation and Maintenance 20–15	
	<u>-</u>	
Chapter	5 (Reserved) 20-15	Appendix B Possible Causes of Pump Troubles 20-53
Chapter	6 Electric Drive for Pumps 20-15	) A P. C. D. C 1D 1P
6-1	General	
6-2	Power Source(s)	
	· =	' Index

### **NFPA 20**

### Standard for the Installation of

### Centrifugal Fire Pumps

### 1996 Edition

NOTICE: An asterisk (\*) following the number or letter designating a paragraph indicates explanatory material on that paragraph in Appendix A.

Information on referenced publications can be found in Chapter 12 and Appendix C.

### Chapter 1 Introduction

1-1 Scope. This standard deals with the selection and installation of pumps supplying water for private fire protection. Items considered include water supplies; suction, discharge, and auxiliary equipment; power supplies; electric drive and control; internal combustion engine drive and control; steam turbine drive and control; and acceptance tests and operation. This standard does not cover system water supply capacity and pressure requirements (see A-2-1.1), nor does it cover requirements for periodic inspection, testing, and maintenance of fire pump systems. (See NFPA 25, Standard for the Inspection, Testing, and Maintenance of Water-Based Fire Protection Systems.)

### 1-2 Purpose.

- 1-2.1 The purpose of this standard is to provide a reasonable degree of protection for life and property from fire through installation requirements for centrifugal fire pumps based upon sound engineering principles, test data, and field experience. This standard includes single-stage and multistage pumps of horizontal or vertical shaft design. Requirements are established for the design and installation of these pumps, pump drivers, and associated equipment. The standard endeavors to continue the excellent record that has been established by centrifugal pump installations and to meet the needs of changing technology. Nothing in this standard is intended to restrict new technologies or alternate arrangements provided the level of safety prescribed by the standard is not lowered.
- 1-2.2 Existing Installations. Where existing pump installations meet the provisions of the standard in effect at the time of purchase, they shall be permitted to remain in use provided they do not constitute a distinct hazard to life or adjoining property.
- 1-3 Other Pumps. Pumps other than those specified in this standard and having different design features shall be permitted to be installed where such pumps are listed by a testing laboratory. They shall be limited to capacities of less than 500 gpm (1892 L/min).

### 1-4\* Approval Required.

- 1-4.1 Centrifugal fire pumps shall be selected based on the conditions under which they are to be installed and used.
- 1-4.2 The pump manufacturer or its designated representative shall be given complete information concerning the water and power supply characteristics.
- 1-4.3 A complete plan and detailed data describing pump, driver, controller, power supply, fittings, suction and dis-

charge connections, and water supply conditions shall be prepared for approval. Each pump, driver, controlling equipment, power supply and arrangement, and water supply shall be approved by the authority having jurisdiction for the specific field conditions encountered.

1-5 Pump Operation. In the event of fire pump operation, qualified personnel shall respond to the fire pump location to determine that the fire pump is operating in a satisfactory manner.

### 1-6 Unit Performance.

- 1-6.1\* The unit, consisting of a pump, driver, and controller, shall perform in compliance with this standard as an entire unit when installed or when components have been replaced.
- 1-6.2 The complete unit shall be field acceptance tested for proper performance in accordance with the provisions of this standard. (See Section 11-2.)
- 1-7 Certified Shop Test. Certified shop test curves showing head capacity and brake horsepower of the pump shall be furnished by the manufacturer to the purchaser. The purchaser shall furnish this data to the authority having jurisdiction.

### 1-8 Definitions.

**Approved.\*** Acceptable to the authority having jurisdiction.

Aquifer. An underground formation that contains sufficient saturated permeable material to yield significant quantities of water.

Aquifer Performance Analysis. A test designed to determine the amount of underground water available in a given field and proper well spacing to avoid interference in that field. Basically, test results provide information concerning transmissibility and storage coefficient (available volume of water) of the aquifer.

Authority Having Jurisdiction. The organization, office, or individual responsible for approving equipment, an installation, or a procedure.

Automatic Transfer Switch. Self-acting equipment for transferring one or more load conductor connections from one power source to another.

**Booster Pump.** A !re pump that takes suction from a public service main or private-use water system for the purpose of increasing the effective water pressure.

**Branch Circuit.** The circuit conductors between the final overcurrent device protecting the circuit and the utilization equipment.

Can Pump. A vertical shaft turbine-type pump in a can (suction vessel) for installation in a pipeline to raise water pressure.

**Centrifugal Pump.** A pump in which the pressure is developed principally by the action of centrifugal force.

Corrosion-Resistant Material. Materials such as brass, copper, monel, stainless steel, or other equivalent corrosion-resistant materials.

Diesel Engine. An internal combustion engine in which the fuel is ignited entirely by the heat resulting from the compression of the air supplied for combustion. The oildiesel engine, which operates on fuel oil injected after compression is practically completed, is the type usually used as a fire pump driver.

**Disconnecting Means.** A device, group of devices, or other means (e.g., the circuit breaker in the fire pump controller) by which the conductors of a circuit can be disconnected from their source of supply.

**Drawdown.** The vertical difference between the pumping water level and the static water level.

**Dripproof Guarded Motor.** A dripproof machine whose ventilating openings are guarded in accordance with the definition for dripproof motor.

Dripproof Motor. An open motor in which the ventilating openings are so constructed that successful operation is not interfered with when drops of liquid or solid particles strike or enter the enclosure at any angle from 0 to 15 degrees downward from the vertical.

Dust-Ignition-Proof Motor. A totally enclosed motor whose enclosure is designed and constructed in a manner that will exclude ignitible amounts of dust or amounts that might affect performance or rating and that will not permit arcs, sparks, or heat otherwise generated or liberated inside of the enclosure to cause ignition of exterior accumulations or atmospheric suspensions of a specific dust on or in the vicinity of the enclosure.

Electric Motors. Electric motors are classified according to mechanical protection and methods of cooling.

End Suction Pump. A single suction pump having its suction nozzle on the opposite side of the casing from the stuffing box and having the face of the suction nozzle perpendicular to the longitudinal axis of the shaft.

**Explosionproof Motor.** A totally enclosed motor whose enclosure is designed and constructed to withstand an explosion of a specified gas or vapor that might occur within it and to prevent the ignition of the specified gas or vapor surrounding the motor by sparks, flashes, or explosions of the specified gas or vapor that might occur within the motor casing.

**Feeder.** All circuit conductors between the service equipment or the source of a separately derived system and the final branch-circuit overcurrent device.

Fire Pump Controller. For the purpose of this standard, a group of devices that serve to govern, in some predetermined manner, the starting and stopping of the fire pump driver as well as monitoring and signaling the status and condition of the fire pump unit.

Fire Pump Unit. An assembled unit consisting of a fire pump, driver, controller, and accessories.

Flexible Connecting Shaft. A device that incorporates two flexible joints and a telescoping element.

Flexible Coupling. A device used to connect the shafts or other torque-transmitting components from a driver to the pump, and that permits minor angular and parallel misalignment as restricted by both the pump and coupling manufacturers.

Flooded Suction. The condition where water flows from an atmospheric vented source to the pump without the average pressure at the pump inlet flange dropping below atmospheric pressure with the pump operating at 150 percent of its rated capacity.

Ground Water. That water that is available from a well, driven into water-bearing subsurface strata (aquifer).

Guarded Motor. An open motor in which all openings giving direct access to live metal or rotating parts (except smooth rotating surfaces) are limited in size by the structural parts or by screens, baffles, grilles, expanded metal, or other means to prevent accidental contact with hazardous parts. Openings giving direct access to such live or rotating parts shall not permit the passage of a cylindrical rod 0.75 in. (19 mm) in diameter.

Head.\* The unit for measuring head shall be the foot (m). The relation between a pressure expressed in pounds per square inch (bars) and a pressure expressed in feet (m) of head is:

head in feet =  $\frac{\text{pressure in psi}}{0.433 \text{ specific gravity}}$ head in feet =  $\frac{\text{pressure in bars}}{0.098 \text{ specific gravity}}$ 

**Horizontal Pump.** A pump with the shaft normally in a horizontal position.

Horizontal Split-Case Pump. A centrifugal pump characterized by a housing that is split parallel to the shaft.

In-Line Pump. A centrifugal pump whose drive unit is supported by the pump having its suction and discharge flanges on approximately the same centerline.

Internal Combustion Engine. Any engine in which the working medium consists of the products of combustion of the air and fuel supplied. This combustion usually is effected within the working cylinder but can take place in an external chamber.

Isolating Switch. A switch intended for isolating an electric circuit from its source of power. It has no interrupting rating and it is intended to be operated only after the circuit has been opened by some other means.

Listed.\* Equipment or materials included in a list published by an organization acceptable to the authority having jurisdiction and concerned with product evaluation that maintains periodic inspection of production of listed equipment or materials and whose listing states either that the equipment or material meets appropriate standards or has been tested and found suitable for use in a specified manner.

**Manual Transfer Switch.** A switch operated by direct manpower for transferring one or more load conductor connection from one power source to another.

Maximum Pump Brake Horsepower. The maximum brake horsepower required to drive the pump at rated speed. The pump manufacturer determines this by shop test under expected suction and discharge conditions. Actual field conditions can vary from shop conditions.

Net Positive Suction Head — NPSH (h<sub>sv</sub>). The total suction head in feet (m) of liquid absolute, determined at the suction nozzle, and referred to datum less the vapor pressure of the liquid in feet (m) absolute.

Open Motor. A motor having ventilating openings that permit passage of external cooling air over and around the windings of the motor. Where applied to large apparatus without qualification, the term designates a motor having no restriction to ventilation other than that necessitated by mechanical construction.

Pumping Water Level. The level, with respect to the pump, of the body of water from which it takes suction when the pump is in operation. Measurements are made the same as with the static water level.

Service. The conductors and equipment for delivering energy from the electricity supply system to the wiring system of the premises served. (See NFPA 70, National Electrical Code®, Article 100.)

Service Equipment. The necessary equipment, usually consisting of a circuit breaker or switch and fuses, and their accessories, located near the point of entrance of supply conductors to a building or other structure, or an otherwise defined area, and intended to constitute the main control and means of cutoff of the supply. (See NFPA 70, National Electrical Code, Article 100.)

Service Factor. The service factor of an ac motor is a multiplier that, when applied to the rated horsepower, indicates a permissible horsepower loading that can be carried at the rated voltage, frequency, and temperature. The multiplier 1.15 indicates that the motor is permitted to be overloaded to 1.15 times the rated horsepower.

Shall. Indicates a mandatory requirement.

**Should.** Indicates a recommendation or that which is advised but not required.

Standard. A document containing only mandatory provisions using the word "shall" to indicate requirements. Explanatory material may be included only in the form of "fine-print" notes (FPN), in footnotes, or in an appendix.

Static Water Level. The level, with respect to the pump, of the body of water from which it takes suction when the pump is not in operation. For vertical shaft turbine-type pumps, the distance to the water level is measured vertically from the horizontal centerline of the discharge head or tee.

Total Discharge Head (hd). The reading of a pressure gauge at the discharge of the pump, converted to feet (m) of liquid, and referred to datum, plus the velocity head at the point of gauge attachment.

Total Head (H), Horizontal Pumps.\* The measure of the work increase per pound (kg) of liquid, imparted to the liquid by the pump, and therefore the algebraic difference between the total discharge head and the total suction head. Total head, as determined on test where suction lift exists, is the sum of the total discharge head and total suction lift. Where positive suction head exists, the total head is the total discharge head minus the total suction head.

Total Head (H), Vertical Turbine Pumps.\* The distance from the pumping water level to the center of the discharge gauge, plus the total discharge head.

Total Rated Head. The total head, defined above, developed at rated capacity and rated speed for either a horizontal splitcase or a vertical shaft turbine-type pump.

Total Suction Head (hs). Suction head exists where the total suction head is above atmospheric pressure. Total suction head, as determined on test, is the reading of a gauge at the suction of the pump, converted to feet (m) of liquid, and referred to datum, plus the velocity head at the point of gauge attachment.

Total Suction Lift (hl). Suction lift exists where the total suction head is below atmospheric pressure. Total suction lift, as determined on test, is the reading of a liquid manometer at the suction nozzle of the pump, converted to feet (m) of liquid, and referred to datum, minus the velocity head at the point of gauge attachment.

Totally Enclosed Fan-Cooled Motor. A totally enclosed motor equipped for exterior cooling by means of a fan or fans integral with the motor but external to the enclosing parts.

Totally Enclosed Motor. A motor so enclosed as to prevent the free exchange of air between the inside and the outside of the case but not sufficiently enclosed to be termed airtight.

Totally Enclosed Nonventilated Motor. A totally enclosed motor that is not equipped for cooling by means external to the enclosing parts.

Velocity Head (hv). The velocity head shall be figured from the average velocity (v) obtained by dividing the flow in cubic feet per second (m³/s) by the actual area of pipe cross section in square feet (m²) and determined at the point of the gauge connection.

Velocity head is expressed by the formula:

$$h_v = \frac{v^2}{2g}$$

Where g = the acceleration due to gravity and is 32.17 ft per second per second (9.807 m/s<sup>2</sup>) at sea level and 45 degrees latitude, and where v = velocity in the pipe in feet per second (m/s).

Vertical Lineshaft Turbine Pump. A vertical shaft centrifugal pump with rotating impeller or impellers and with discharge from the pumping element coaxial with the shaft. The pumping element is suspended by the conductor system, which encloses a system of vertical shafting used to transmit power to the impellers, the prime mover being external to the flow stream.

Wet Pit. A timber, concrete, or masonry enclosure having a screened inlet kept partially filled with water by an open body of water such as a pond, lake, or stream.

1-8.1 Additional Definitions. Additional applicable definitions can be found in the latest edition of Hydraulics Institute Standards for Centrifugal, Rotary and Reciprocating Pumps and NFPA 70, National Electrical Code.

1-9 Units. Metric units of measurement in this standard are in accordance with the modernized metric system known as the International System of Units (SI). Two units (liter and bar), outside of but recognized by SI, are commonly used in international fire protection. These units are listed in Table 1-9 with conversion factors.

1-9.1 If a value for measurement as given in this standard is followed by an equivalent value in other units, the first stated is to be regarded as the requirement. A given equivalent value is considered to be approximate.

1-9.2 The conversion procedure for the SI units has been to multiply the quantity by the conversion factor and then round the result to the approximate number of significant digits.

Table 1-9

Name of Unit	Unit Symbol	Conversion Factor
meter	m	1  ft = 0.3048  m
millimeter	mm	1  in. = 25.4  mm
liter	L	1  gal = 3.785  L
cubic decimeter	dm <sup>3</sup>	$1 \text{ gal} = 3.785 \text{ dm}^3$
cubic meter	m <sup>5</sup>	$1 \text{ ft}^3 = 0.0283 \text{ m}^3$
pascal	Pa	1  psi = 6894.757  Pa
bar	bar	1  psi = 0.0689  bar
bar	bar	$1  \text{bar} = 10^5  \text{Pa}$

NOTE: For additional conversions and information, see ASTM E 380, Standard for Metric Practice.

### Chapter 2 General

### 2-1 Water Supplies.

- 2-1.1\* The adequacy and dependability of the water source are of primary importance and shall be fully determined, with due allowance for its reliability in the future. (See A-2-1.1.)
- 2-1.2\* Sources. Any source of water that is adequate in quality, quantity, and pressure shall be permitted to provide the supply for a fire pump. Where the water supply from a public service main is not adequate in quality, quantity, or pressure, an alternative water source shall be provided. The adequacy of the water supply shall be determined and evaluated prior to the specification and installation of the fire pump.
- 2-1.3 The minimum water level of a well or wet pit shall be determined by pumping at not less than 150 percent of the fire pump rated capacity.
- 2-1.4\* A stored supply shall be sufficient to meet the demand placed upon it for the expected duration, and a reliable method of replenishing the supply shall be provided.
- 2-1.5 The head available from a water supply shall be figured on the basis of a flow of 150 percent of rated capacity of the fire pump. This head shall be as indicated by a flow test.

### | 2-2 Pumps and Drivers.

- **2-2.1** Centrifugal fire pumps shall be listed for fire protection service.
- **2-2.2** Acceptable drivers for pumps at a single installation are electric motors, diesel engines, steam turbines, or a combination thereof.
- 2-2.3 Except for installations made prior to adoption of the 1974 edition of this standard, dual-drive pump units shall not be used.
- 2-3\* Rated Pump Capacities. Fire pumps shall have the following rated capacities in gpm (L/min) and shall be rated at net pressures of 40 psi (2.7 bars) or more. Pumps for ratings over 5000 gpm (18,925 L/min) are subject to individual review by either the authority having jurisdiction or a listing laboratory.

Table 2-3

gpm	L/min	gpm	L/min	gpm	L/min
25	95	400	1514	2000	7570
50	189	450	1703	2500	9462
100	379	500	1892	3000	11.355
150	568	750	2839	3500	13,247
200	757	1000	3785	4000	15,140
250	946	1250	4731	4500	17,032
300	1136	1500	5677	5000	18,925

2-4 Nameplate. Pumps shall be provided with a name-plate.

### 2-5 Pressure Gauges.

- **2-5.1** A pressure gauge having a dial not less than  $3\frac{1}{2}$  in. (89 mm) in diameter shall be connected near the discharge casting with a  $\frac{1}{4}$ -in. (6.25-mm) gauge valve. The dial shall indicate pressure to at least twice the rated working pressure of the pump but not less than 200 psi (13.8 bars). The face of the dial shall read in pounds per square inch or bars or both with the manufacturer's standard graduations.
- 2-5.2\* A compound pressure and vacuum gauge having a dial not less than  $3\frac{1}{2}$  in. (89 mm) in diameter shall be connected to the suction pipe near the pump with a  $\frac{1}{4}$ -in. (6.25-mm) gauge valve.

Exception: This rule shall not apply to vertical shaft turbine-type pumps taking suction from a well or open wet pit.

The face of the dial shall read in inches (mm) of mercury (Hg) or pounds per square inch (bars) for the suction range. The gauge shall have a pressure range two times the rated maximum suction pressure of the pump, but not less than 100 psi (7 bars).

| 2-6 Circulation Relief Valve. Each pump(s) shall have an automatic relief valve listed for the fire pump service | installed and set below the shutoff pressure at minimum expected suction pressure. It shall provide flow of sufficient water to prevent the pump from overheating when operating with no discharge. Provisions shall be made for discharge to a drain. Circulating relief valves shall not be tied in with the packing box or drip rim drains.

Minimum size of the automatic relief valve shall be  $\frac{3}{4}$  in. (19.0 mm) for pumps with a rated capacity not exceeding 2500 gpm (9462 L/min), and 1 in. (25.4 mm) for pumps with a rated capacity of 3000 to 5000 gpm (11,355 to 18,925 L/min).

Exception: This rule shall not apply to engine-driven pumps for which engine cooling water is taken from the pump discharge.

### 2-7\* Equipment Protection.

2-7.1\* The fire pump, driver, and controller shall be protected against possible interruption of service through damage caused by explosion, fire, flood, earthquake, rodents, insects, windstorm, freezing, vandalism, and other adverse conditions.

2-7.2 Suitable means shall be provided for maintaining the temperature of a pump room or pump house, where required, above 40°F (5°C).

Exception: See 8-6.5 for higher temperature requirements for internal combustion engines.

- 2-7.3 Artificial light shall be provided in a pump room or pump house.
- 2-7.4 Emergency lighting shall be provided by fixed or portable battery-operated lights, including flashlights. Emergency lights shall not be connected to an enginestarting battery.
- 2-7.5 Provision shall be made for ventilation of a pump room or pump house.
- 2-7.6\* Floors shall be pitched for adequate drainage of scaping water away from critical equipment such as the pump, driver, controller, etc. The pump room or pump house shall be provided with a floor drain that will discharge to a frost-free location.
- 2-7.7 Guards. Guards shall be provided for flexible couplings and flexible connecting shafts to prevent rotating elements from causing injury to personnel.

### 2-8 Pipe and Fittings.

- 2-8.1\* Steel pipe shall be used aboveground except for connection to underground suction and underground discharge piping. Where corrosive water conditions exist, steel suction pipe shall be galvanized or painted on the inside prior to installation with a paint recommended for submerged surfaces. Thick bituminous linings shall not be used.
- **2-8.2** Sections of steel piping shall be joined by means of screwed, flanged (flanges welded to pipe are preferred), mechanical grooved joints, or other approved fittings.

Exception: Slip-type fittings shall be permitted to be used where installed as required by 2-9.6 and where the piping is mechanically secured to prevent slippage.

- 2-8.3 All provisions for welded pipe shall be in accordance with NFPA 13, Standard for the Installation of Sprinkler Systems.
- 2-8.4\* Torch-cutting or welding in the pump house shall be permitted as a means of modifying or repairing pump house piping when it is performed in accordance with NFPA 51B, Standard for Fire Prevention in Use of Cutting and Welding Processes.

### 2-9 Suction Pipe and Fittings.

- 2-9.1\* The suction components shall consist of all pipe, valves, and fittings from the pump suction flange to the connection to the public or private water service main, storage tank, or reservoir, etc., that feeds water to the pump. Where pumps are installed in series, the suction pipe for the subsequent pump(s) shall begin at the system side of the discharge valve of the previous pump.
- | 2-9.2 Suction pipe shall be installed and tested in accordance with NFPA 24, Standard for the Installation of Private Fire Service Mains and Their Appurtenances.

2-9.3 Suction Size. The size of the suction pipe for a single pump or of the suction header pipe for multiple pumps (operating together) shall be such that, with all pumps operating at 150 percent of rated capacity, the gauge pressure at the pump suction flanges shall be 0 psi (0 bars) or higher. The suction pipe shall be sized such that, with the pump(s) operating at 150 percent of rated capacity, the velocity in the suction pipe does not exceed 15 ft/sec (4.57 m/s). The size of that portion of the suction pipe located within 10 pipe diameters upstream of the pump suction flange shall be not less than that specified in Table 2-20.

Exception: Where the water supply is a suction tank with its base at or above the same elevation as the pump, the gauge pressure at the pump suction flange shall be permitted to drop to -3 psig (0.14 kPa.)

- **2-9.4\* Pumps with Bypass.** Where the suction supply is of sufficient pressure to be of material value without the pump, the pump shall be installed with a bypass. (See Figure A-2-9.4.) The size of the bypass shall be at least as large as the pipe size required for discharge pipe as specified in Table 2-20.
- 2-9.5\* Valves. A listed OS&Y gate valve shall be installed in the suction pipe. A butterfly valve shall not be installed in the suction pipe within 50 ft (16 m) upstream of the pump suction flange.

### 2-9.6\* Installation.

- (a) Suction pipe shall be laid carefully to avoid air leaks and air pockets, either of which may seriously affect the operation of the pump. (See Figure A-2-9.6.)
- (b) Suction pipe shall be installed below the frost line or in frostproof casings. Where pipe enters streams, ponds, or reservoirs, special attention shall be given to prevent freezing either underground or underwater.
- (c) Elbows with a centerline plane parallel to a horizontal split-case pump shaft shall be avoided. (See Figure A-2-9.6.)

Exception: Elbows with a centerline plane parallel to a horizontal split-case pump shaft shall be permitted where the distance between the flanges of the pump suction intake and the elbow is greater than 10 times the suction pipe diameter.

- (d) Where the suction pipe and pump suction flange are not of the same size, they shall be connected with an eccentric tapered reducer or increaser installed in such a way as to avoid air pockets. (See Figure A-2-9.6.)
- (e) Where the pump and its suction supply are on separate foundations with rigid interconnecting pipe, the pipe shall be provided with strain relief. (See Figure A-3-3.1.)
- **2-9.7** Multiple Pumps. Where a single suction pipe supplies more than one pump, the suction pipe layout at the pumps shall be arranged so that each pump will receive its proportional supply.
- 2-9.8\* Suction Screening. Where the water supply is obtained from an open source such as a pond or wet pit, the passage of materials that might clog the pump shall be obstructed. Double removable intake screens shall be provided at the suction intake. Below minimum water level these screens shall have an effective net area of openings of 1 in.<sup>2</sup> (645 mm<sup>2</sup>) for each gpm (3.785 L/min) at 150 percent of rated pump capacity. Screens shall be so arranged that

GENERAL 20–9

they can be cleaned or repaired without disturbing the suction pipe. A brass, copper, monel, stainless steel, or other equivalent corrosion-resistant metallic material wire screen of  $\frac{1}{2}$ -in. (12.7-mm) mesh and No. 10 B. & S. gauge wire shall be secured to a metal frame sliding vertically at the entrance to the intake. The overall area of this particular screen shall be 1.6 times the net screen opening area. (See screen details in Figure A-4-2.2.2.)

### 2-9.9\* Devices in Suction Piping.

(a) No device or assembly (including, but not limited to, backflow prevention devices or assemblies) that will stop, restrict the starting, or restrict the discharge of a fire pump or pump driver shall be installed in the suction piping.

| Exception No 1: Except as specified in 2-9.5.

- Exception No 2: Check valves and backflow prevention devices and assemblies shall be permitted where required by other NFPA standards or the authority having jurisdiction.
- Exception No. 3: Flow control valves that are listed for fire pump service and that are suction pressure sensitive shall be permitted where the authority having jurisdiction requires positive pressure to be maintained on the suction piping.
- (b) Suitable devices shall be permitted to be installed in the suction supply piping or stored water supply and arranged to activate an alarm if the pump suction pressure or water level falls below a predetermined minimum.
- **2-9.10 Vortex Plate.** For pump(s) taking suction from a stored water supply, a vortex plate shall be installed at the entrance to the suction pipe. (For example, see Figure A-3-3.1 and the Hydraulics Institute Standards for Centrifugal, Rotary and Reciprocating Pumps.)

### 2-10 Discharge Pipe and Fittings.

- 2-10.1 The discharge components shall consist of pipe, valves, and fittings extending from the pump discharge flange to the system side of the discharge valve.
- **2-10.2** The pressure rating of the discharge components shall be adequate for the maximum working pressure but not less than the rating of the fire protection system. Steel pipe with flanges (flanges welded to the pipe are preferred), screwed joints, or mechanical grooved joints shall be used aboveground. All pump discharge pipe shall be hydrostatically tested in accordance with NFPA 13, Standard for the Installation of Sprinkler Systems, and NFPA 24, Standard for the Installation of Private Fire Service Mains and Their Appurtenances.
- 2-10.3\* The size of pump discharge pipe and fittings shall be not less than that given in Table 2-20.
- **2-10.4\*** A listed check valve shall be installed in the pump discharge assembly.
- **2-10.5** A listed indicating gate or butterfly valve shall be installed on the fire protection system side of the pump discharge check valve. Where pumps are installed in series, a butterfly valve shall not be installed between pumps.
- **2-11\* Valve Supervision.** Where provided, the suction valve, discharge valve, bypass valves, and isolation valves on the backflow prevention device or assembly shall be supervised open by one of the following methods:
- (a) Central station, proprietary, or remote station signaling service;

- (b) Local signaling service that will cause the sounding of an audible signal at a constantly attended point;
  - (c) Locking valves open;
- (d) Sealing of valves and approved weekly recorded inspection where valves are located within fenced enclosures under the control of the owner.

Exception: The test outlet control valves shall be supervised closed.

2-12\* Protection of Piping Against Damage Due to Movement. A clearance of not less than 1 in. (25.4 mm) shall be provided around pipes that pass through walls or floors.

### 2-13 Relief Valve.

- 2-13.1\* Where the pump shutoff pressure plus the static suction pressure exceeds the pressure for which the system components are rated, relief valves shall be required.
- 2-13.2 The relief valve size shall not be less than that given in Table 2-20. (Refer also to 2-13.8 and A-2-13.8 for conditions affecting size.)
- 2-13.3 The relief valve shall be located between the pump and the pump discharge check valve and shall be so attached that it can be readily removed for repairs without disturbing the piping.
- 2-13.4 Pressure relief valves are of two types: (1) the spring-loaded and (2) the pilot-operated diaphragm type.
- 2-13.4.1 Pilot-operated pressure relief valves, where attached to vertical shaft turbine pumps, shall be arranged to prevent relieving of water at water pressures less than the pressure relief setting of the valve.
- 2-13.5\* The relief valve shall discharge into an open pipe or into a cone or funnel secured to the outlet of the valve. Water discharge from the relief valve shall be readily visible or easily detectable by the pump operator. Splashing of water into the pump room shall be avoided. If a closed-type cone is used, it shall be provided with means for detecting motion of water through the cone. If the relief valve is provided with means for detecting motion (flow) of water through the valve, then cones or funnels at its outlet shall not be required.
- **2-13.6** The relief valve shall not be piped to the pump suction or supply connection.
- 2-13.7 The relief valve discharge pipe from an open cone shall be of a size not less than that given in Table 2-20. If the pipe employs more than one elbow, the next larger pipe size shall be used.
- 2-13.8\* Where the relief valve must be piped back to the source of supply, the relief valve and piping shall have sufficient capacity to prevent pressure from exceeding that for which system components are rated.
- 2-13.9\* Where the supply of water to the pump is taken from a suction reservoir of limited capacity, the drain pipe shall discharge into the reservoir at a point as far from the pump suction as is necessary to prevent the pump from drafting air introduced by the drain pipe discharge.
- 2-13.10 A shutoff valve shall not be installed in the relief valve supply or discharge piping.

### | 2-14 Waterflow Test Devices.

### 2-14.1 General.

- | 2-14.1.1 A fire pump installation and fire protection system(s) shall have the ability to test the pump and the suction supply at the maximum flow available from the fire pump.
  - 2-14.1.2\* Where water usage or discharge is not permitted for the duration of the test specified in Chapter 11, the outlet shall be used to test the pump and suction supply and determine that the system is operating in accordance with the design. The flow shall continue until flow has stabilized. (See 11-2.6.3.)

### 2-14.2 Meters.

- 2-14.2.1\* Metering devices or fixed nozzles for pump testing shall be listed. They shall be capable of water flow of not less than 175 percent of pump-rated capacity.
- 2-14.2.2 All of the meter system piping shall be sized as specified by the meter manufacturer but not less than the meter device sizes shown in Table 2-20.
- 2-14.2.3 The minimum size meter for a given pump capacity shall be permitted to be used where the meter system piping does not exceed 100 ft (30 m) equivalent length. Where meter system piping exceeds 100 ft (30 m) (length of straight pipe plus equivalent length in fittings, elevation, and loss through meter), the next larger size of piping shall be used to minimize friction loss. The primary element shall be suitable for that pipe size and pump rating. The readout instrument shall be sized for the pump-rated capacity. (See Table 2-20.)

### 2-14.3 Hose Valves.

- 2-14.3.1\* Hose valves shall be listed. The number and size of hose valves used for pump testing shall be as specified in Table 2-20. Hose valves shall be mounted on a hose valve header and supply piping shall be sized per Table 2-20.
- 2-14.3.2 Hose valve(s) shall have the NH standard external thread for the valve size specified, as specified in NFPA 1963, Standard for Fire Hose Connections.

Exception: Where local fire department connections do not conform to NFPA 1963, the authority having jurisdiction shall designate the threads to be used.

- **2-14.3.3** Where the hose valve header is located outside or at a distance from the pump and there is danger of freezing, a listed indicating or butterfly gate valve and drain valve or ball drip shall be located in the pipe line to the hose valve header. The valve shall be at a point in the line close to the pump. (See Figure A-3-3.1.)
- **2-14.3.4** Where the pipe between the hose valve header and connection to the pump discharge pipe is over 15 ft (4.5 m) in length, the next larger pipe size shall be used.

Exception: This pipe is permitted to be sized by hydraulic calculations based on a total flow of 150 percent of rated pump capacity. This calculation shall include friction loss for the total length of pipe plus equivalent lengths of fittings, control valve, and hose valves, plus elevation loss, from the pump discharge flange to the hose valve outlets. The installation shall be proven by a test flowing the maximum water available.

### 2-15 Power Supply Dependability.

- 2-15.1 Electric Supply. Careful consideration shall be given in each case to the dependability of the electric supply system and the wiring system. This shall include the possible effect of fire on transmission lines either in the property or in adjoining buildings that might threaten the property.
- 2-15.2 Steam Supply. Careful consideration shall be given in each case to the dependability of the steam supply and the steam supply system. This shall include the possible effect of fire on transmission piping either in the property or in adjoining buildings that might threaten the property.

### 2-16 Shop Tests.

- **2-16.1** Each individual pump shall be tested at the factory to provide detailed performance data and to demonstrate its compliance with specifications.
- 2-16.2 Before shipment from the factory, each pump shall be hydrostatically tested by the manufacturer for a period of time not less than 5 minutes. The test pressure shall not be less than 1½ times the sum of the pump's shutoff head plus its maximum allowable suction head, but in no case shall it be less than 250 psi (17 bars). Pump casings shall be essentially tight at the test pressure. During the test, no objectionable leakage shall occur at any joint. In the case of vertical turbine-type pumps, both the discharge casting and pump bowl assembly shall be tested.
- 2-17\* Pump Shaft Rotation. Pump shaft rotation shall be determined and correctly specified when ordering fire pumps and equipment involving that rotation.
- 2-18\* Alarms. Various sections of this standard specify alarms to call attention to improper conditions that can exist in the complete fire pump equipment.

### 2-19\* Pressure Maintenance (Jockey or Make-Up) Pumps.

- 2-19.1 Pressure maintenance pumps shall have rated capacities not less than any normal leakage rate. They shall have discharge pressure sufficient to maintain the desired fire protection system pressure.
- 2-19.2 A check valve shall be installed in the discharge pipe.
- **2-19.3\*** Indicating butterfly or gate valves shall be installed in such places as needed to make the pump, check valve, and other miscellaneous fittings accessible for repair. (See Figure A-2-19.3.)
- 2-19.4\* Where a centrifugal-type pressure maintenance pump has a shutoff pressure exceeding the working pressure rating of the fire protection equipment, or where a turbine | vane (peripheral) type of pump is used, a relief valve sized to prevent overpressuring of the system shall be installed on the pump discharge to prevent damage to the fire protection system. Running period timers shall not be used where jockey pumps are utilized that have the capability of exceeding the working pressure of the fire protection systems.
- | 2-19.5 The primary or standby fire pump shall not be used as a pressure maintenance pump.
- 2-19.6 Steel pipe shall be used for suction and discharge piping on jockey pumps. This includes packaged prefabricated systems.

Table 2-20 Summary of Fire Pump Data

Minimum Pipe Sizes (Nominal)							
Pump Rating gpm (L/min)	Suction in. <sup>1,2</sup>	Discharge in. <sup>1</sup>	Relief Valve in.	Relief Valve Discharge in.	Meter Device in.	Number and Size of Hose Valves in.	Hose Heade Supply in.
25 (95)	1	1	3/4	1	1 1/4	1 — 1 1/2	1
50 (189)	1 1/2	144	1 1/4	1 1/2	2	$1 - 1\frac{1}{2}$	1 1/2
100 (379)	2	2	11/2	2	242	$1 - 2\frac{1}{2}$	21/2
150 (568)	242	242	2	$2\frac{1}{2}$	3	$1 - 2\frac{1}{2}$	21/2
200 (757)	3	3	2	21/2	3	1 2 1/2	21/2
250 (946)	342	3	2	21/2	31/2	1 — 2 1/2	3
300 (1136)	4	4	242	342	31/2	$1 - 2\frac{1}{2}$	3
400 (1514)	4	4	3	5	4	2 - 2 1/2	4
450 (1703)	5	5	3	5	4	$2 - 2 \frac{1}{2}$	4
500 (1892)	5	5	3	5	5	2 2 1/2	4
750 (2839)	. 6	6	4	6	5	3 - 2 1/2	6
1000 (3785)	8	6	4	8	6	$4 - 2\frac{1}{2}$	6
1250 (4731)	8	8	6	8	6	$6 - 2\frac{1}{2}$	8
1500 (5677)	8	8	6	8	8	6 - 21/2	8
2000 (7570)	10	10	6	10	8	6 - 2 1/2	8
2500 (9462)	10	10	6	10	8	8-21/2	10
3000 (11,355)	12	12	8	12	8	$12 - 2\frac{1}{2}$	10
3500 (13,247)	12	12	8	12	10	12 - 21/2	12
4000 (15,140)	14	12	8	14	10	$16 - 2\frac{1}{2}$	12
4500 (17,032)	16	14	8	14	10	$16 - 2\frac{1}{2}$	12
5000 (18,925)	16	14	8	14	10	$20 - 2\frac{1}{2}$	12

NOTE 1: Actual diameter of pump flange is permitted to be different from pipe diameter.

NOTE 2: Applies only to that portion of suction pipe specified in 2-9.3.

### 2-20 Summary of Fire Pump Data. See Table 2-20.

### 2-21 Backflow Preventers and Check Valves.

- 2-21.1 Check valves and backflow prevention devices and assemblies shall be listed for fire protection service.
- 2-21.2 Where the backflow prevention device or assembly incorporates a relief valve, the relief valve shall discharge to a drain appropriately sized for the maximum anticipated flow. An air gap shall be provided in accordance with the manufacturer's recommendations. Water discharge from the relief valve shall be readily visible or easily detectable. Performance of the above requirements shall be documented by engineering calculations and tests.
- 2-21.3 Where located upstream of the pump, check valves and backflow prevention devices or assemblies shall be located a minimum of 10 pipe diameters from the pump suction flange.
- 2-21.4 Where the authority having jurisdiction requires the installation of a backflow prevention device or assembly in connection with the pump, special consideration shall be given to the increased pressure loss resulting from the installation. Under these circumstances, it is critical to ensure the final arrangement shall provide effective pump performance with a minimum suction pressure of 0 psi (0 bar) at the gauge at 150 percent of rated capacity. Determination of effective pump performance shall be documented by engineering calculations and tests.

### 2-22 Earthquake Protection.

2-22.1\* Where local codes require seismic design, the fire pump, driver, diesel fuel tank (where installed), and fire

pump controller shall be attached to their foundations with materials capable of resisting lateral movement of horizontal forces equal to one-half of the weight of the equipment.

Exception: Where the authority having jurisdiction requires horizontal force factors other than 0.5, Exception No. 2 to 4-14.4.3.5.3 of NFPA 13, Standard for the Installation of Sprinkler Systems, shall apply.

- 2-22.2 Pumps with high centers of gravity (such as vertical in-line pumps) shall be mounted at their base and braced above their center of gravity in accordance with the requirements of 2-22.1.
- 2-22.3 A flexible coupling shall be installed at the base of the system riser.

### Chapter 3 Horizontal and In-Line Pumps

### 3-1 General.

An appeal has been filed on the following section. See page 2.

- 3-1.1 Types. Horizontal pumps shall be of the split-case, end-suction, or in-line design.
- 3-1.2 Application. The horizontal split-case pump in horizontal or vertical position, and end-suction and in-line pumps shall not be used where a static suction lift is involved.

### 3-2 Factory and Field Performance.

- 3-2.1\* Characteristics. Pumps shall furnish not less than 150 percent of rated capacity at not less than 65 percent of total rated head. The shutoff head shall not exceed 140 percent of rated head for any type pump. (See Figure A-3-2.1.)
- **3-2.2** Upon completion of the entire fire pump installation, an acceptance test shall be conducted in accordance with the provisions of this standard.

### 3-3 Fittings.

- 3-3.1\* Where necessary, the following fittings for the pump shall be provided by the pump manufacturer or an authorized representative (see Figure A-3-3.1):
  - (a) Automatic air release,
  - (b) Circulation relief valve, and
  - (c) Pressure gauges.
- **3-3.2** Where necessary, the following fittings shall be provided (see Figure A-3-3.1):
  - (a) Eccentric tapered reducer at suction inlet,
  - (b) Hose valve manifold with hose valves,
  - (c) Flow measuring device, and
  - (d) Relief valve and discharge cone.
- **3-3.3** Automatic Air Release. Pumps that are automatically controlled shall be provided with a listed float-operated air release not less than  $\frac{1}{2}$  in. (12.7 mm) in size, to automatically release air from the pump.

Exception: This shall not be required for end suction pumps with top centerline discharge or in-line pumps.

### 3-4 Foundation and Setting.

| 3-4.1\* The pump and driver shall be mounted on a common grouted base plate.

Exception: In-line pumps shall be permitted to be mounted on a base attached to the pump only.

- 3-4.2 The base plate shall be securely attached to a solid foundation in such a way that proper pump and driver shaft alignment will be ensured.
- 3-4.3\* The foundation shall be sufficiently substantial to form a permanent and rigid support for the base plate.
- **3-4.4** The base plate, with pump and driver mounted on it, shall be set level on the foundation.

### 3-5\* Connection to Driver and Alignment.

**3-5.1** The pump and driver shall be connected by a flexible coupling or flexible connecting shaft listed for this service. For end suction pumps, the coupling shall accommodate sufficient space between the pump and driver shafts to permit removal of the pump's impeller.

Exception: This shall not apply to close-coupled vertical in-line pumps.

**3-5.2** Pumps and drivers shall be aligned in accordance with the coupling and pump manufacturers' specifications and the *Hydraulics Institute Standards for Centrifugal, Rotary and Reciprocating Pumps.* (See A-3-5.) The operating angle for the flexible connecting shaft shall not exceed the maximum recommended by the manufacturer for the speed and horsepower transmitted.

Exception: This shall not apply to close-coupled vertical in-line pumps.

### Chapter 4 Vertical Shaft Turbine-Type Pumps

### 4-1\* General.

- 4-1.1\* Suitability. The vertical shaft turbine-type pump is particularly suitable for fire pump service where the water source is located below ground and where it would be difficult to install any other type of pump below the minimum water level. It was originally designed for installation in drilled wells, but is permitted to be used to lift water from lakes, streams, open swamps, and other subsurface sources. Both oil-lubricated enclosed-line-shaft and water-lubricated open-line-shaft pumps are used. Some health departments object to the use of oil-lubricated pumps; such authorities shall be consulted before proceeding with oil-lubricated design.
- 4-1.2 Maximum Depth. Fire pumps shall not be installed in a well where the pumping water level exceeds 200 ft (61 m) from the surface of the ground when pumping at 150 percent of rated capacity. In all applications the authority having jurisdiction shall be supplied with data on the drawdown characteristics of the well and the pump performance. The available discharge pressure at the discharge flange of the vertical pump can be determined from this data. (See Section 1-8 for definitions.)
- **4-1.3 Characteristics.** Pumps shall furnish not less than 150 percent of rated capacity at a total head of not less than 65 percent of the total rated head. The total shutoff head shall not exceed 140 percent of the total rated head on vertical turbine pumps. (See Figure A-3-2.1.)

### 4-2 Water Supply.

### 4-2.1 Source.

- **4-2.1.1\*** The water supply shall be adequate, dependable, and acceptable to the authority having jurisdiction.
- **4-2.1.2\*** The acceptance of a well as a water supply source shall be dependent upon satisfactory development of the well and establishment of satisfactory aquifer characteristics. (See Section 1-8 for definitions.)

### 4-2.2 Pump Submergence.

- 4-2.2.1\* Well Installations. Proper submergence of the pump bowls shall be provided for reliable operation of the fire pump unit. Submergence of the second impeller from the bottom of the pump bowl assembly shall be not less than 10 ft (3 m) below the pumping water level at 150 percent of rated capacity. (See Figure A-4-2.2.1.) The submergence shall be increased by 1 ft (0.3 m) for each 1000 ft (305 m) of elevation above sea level.
- 4-2.2.2\* Wet Pit Installations. To provide submergence for priming, the elevation of the second impeller from the bottom of the pump bowl assembly shall be such that it is below the lowest pumping water level in the open body of water supplying the pit. For pumps with rated capacities of 2000 gpm (7570 L/min) or greater, additional submergence is required to prevent the formation of vortices and to provide required NPSH available to prevent excessive cavitation. The required submergence shall be obtained from the pump manufacturer. (See the Hydraulics Institute Standards for Centrifugal, Rotary and Reciprocating Pumps.)

### 4-2.3 Well Construction.

- **4-2.3.1** It shall be the responsibility of the groundwater supply contractor to perform the necessary groundwater investigation to establish the reliability of the supply, to develop a well to produce the required supply, and to perform all work and install all equipment in a thorough and workmanlike manner.
- **4-2.3.2** The vertical turbine-type pump is designed to operate in a vertical position with all parts in correct alignment. The well therefore shall be of ample diameter and sufficiently plumb to receive the pump.

### 4-2.4 Unconsolidated Formations (Sands and Gravels).

- 4-2.4.1 All casings shall be of steel of such diameter and installed to such depths as the formation might justify and best meet the conditions. Both inner and outer casings shall have a minimum wall thickness of 0.375 in. (9.5 mm). Inner casing diameter shall be not less than 2 in. (51 mm) larger than the pump bowls.
- **4-2.4.2** Outer casing shall extend down to approximately the top of the water-bearing formation. The inner casing of lesser diameter and the well screen shall extend as far into the formation as the water-bearing stratum might justify and as best meets the conditions.
- 4-2.4.3 The well screen is a vital part of the construction and careful attention shall be given to its selection. It shall be the same diameter as the inner casing and of the proper length and percent open area to provide an entrance velocity not exceeding 0.15 ft (46 mm) per second. The screen shall be made of a corrosion- and acid-resistant material, such as stainless steel or monel; monel shall be used where it is anticipated that the chloride content of the well water will exceed 1000 parts per million. The screen shall have adequate strength to resist the external forces that will be applied after it is installed and to minimize the likelihood of damage during the installation.
- **4-2.4.4** The bottom of the well screen shall be sealed properly with a plate of the same material as the screen. The sides of the outer casing shall be sealed by the introduction of neat cement placed under pressure from the bottom to the top. Cement shall be allowed to set for a minimum of 48 hours before drilling operations are continued.
- 4-2.4.5 The immediate area surrounding the well screen not less than 6 in. (152 mm) shall be filled with clean and well-rounded gravel. This gravel shall be of such size and quality as will create a gravel filter to ensure sand-free production and a low velocity of water leaving the formation and entering the well.
- **4-2.4.6** Wells. Wells for fire pumps not exceeding 450 gpm (1703 L/min) developed in unconsolidated formations without an artificial gravel pack (tubular wells) shall be acceptable sources of water supply for fire pumps not exceeding 450 gpm (1703 L/min). They shall comply with all of the requirements of 4-2.3 and all of 4-2.4, except 4-2.4.4 and 4-2.4.5.
- **4-2.5\*** Consolidated Formations. Where the drilling penetrates unconsolidated formations above the rock, surface casing shall be installed, seated in solid rock, and cemented in place.
- 4-2.6 Developing a Well. Developing a new well and cleaning it of sand or rock particles (not to exceed five parts per million) shall be the responsibility of the ground water

supply contractor. Such development shall be performed with a test pump and not a fire pump. Freedom from sand shall be determined when the test pump is operated at 150 percent of rated capacity of the fire pump for which the well is being prepared.

4-2.7\* Test and Inspection of Well. A test to determine the water production of the well shall be made. An acceptable water measuring device such as an orifice, a venturi meter, or a calibrated pitot tube shall be used. The test shall be witnessed by a representative of the customer, contractor, and authority having jurisdiction, as required. It shall be continuous for a period of at least 8 hours at 150 percent of the rated capacity of the fire pump, with 15-minute interval readings over the period of the test. The test shall be evaluated with consideration given to the effect of other wells in the vicinity and any possible seasonal variation in the water table at the well site. Test data shall describe the static water level and the pumping water level at 100 percent and 150 percent, respectively, of the rated capacity of the fire pump for which the well is being prepared. All existing wells within a 1000-ft (305-m) radius of the fire well shall be monitored throughout the test period.

### 4-3 Pump.

**4-3.1\* Head.** The pump head shall be either the aboveground or belowground discharge type. It shall be designed to support the driver, pump, column assembly, bowl assembly, maximum down thrust, and the oil tube tension nut or packing container.

### 4-3.2 Column.

- 4-3.2.1 The pump column shall be furnished in sections not exceeding a nominal length of 10 ft (3 m), shall be not less than the weight specified in Table 4-3.2.1, and shall be connected by threaded-sleeve couplings or flanges. The ends of each section of threaded pipe shall be faced parallel and machined with threads to permit the ends to butt so as to form accurate alignment of the pump column. All column flange faces shall be parallel and machined for rabbet fit to permit accurate alignment.
- **4-3.2.2** Where the static water level exceeds 50 ft (15 m) belowground, oil-lubricated-type pumps shall be used. (See Figure A-4-1.1.)
- 4-3.2.3 Where the pump is of the enclosed line shaft oillubricated type, the shaft enclosing tube shall be furnished in interchangeable sections not over 10 ft (3 m) in length of extra-strong pipe. An automatic sight feed oiler shall be provided on a suitable mounting bracket with connection to the shaft tube for oil-lubricated pumps. (See Figure A-4-1.1.)
- **4-3.2.4** The pump line shafting shall be sized so critical speed shall be 25 percent above and below the operating speed of the pump. Operating speed shall include all speeds from shutoff to the 150 percent point of the pump, which vary on engine drives.

### 4-3.3 Bowl Assembly.

- **4-3.3.1** The pump bowl shall be of close-grained cast iron, bronze, or other suitable material in accordance with the chemical analysis of the water and experience in the area.
- **4-3.3.2** Impellers shall be of the enclosed type and shall be of bronze or other suitable material in accordance with the chemical analysis of the water and experience in the area.

Table 4-3.2.1 Pump Column Pipe Weights

Nominal Size (ID)	Outside Diameter		Weight per ft (Plain Ends)	Nominal Size (ID)	Outside Diameter		Weight per ft (Plain Ends)
in.	in.	(mm)	lb*	in.	in.	(mm)	lb
6	6.625	168.3	18.97	10	10.75	273.0	31.20
7	7.625	193.7	22.26	12	12.75	323.8	43.77
8	8.625	219.1	24.70	14 OD	14.00	355.6	53.57
9	9.625	244.5	28.33				

<sup>\*</sup>Metric weights in kilograms per meter — 28.230, 33.126, 36.758, 42.159,46.431, 65.137, and 81.209.

### 4-3.4 Suction Strainer.

- **4-3.4.1** A cast or heavy fabricated, corrosion-resistant metal cone or basket-type strainer shall be attached to the suction manifold of the pump. The suction strainer shall have a free area of at least four times the area of the suction connections, and the openings shall be sized to restrict the passage of a  $\frac{1}{2}$ -in. (12.7-mm) sphere.
- **4-3.4.2** For installations in a wet pit, this suction strainer shall be required in addition to the intake screen. (*See Figure A-4-2.2.2.*)

### 4-3.5 Fittings.

- **4-3.5.1** The following fittings shall be required for attachment to the pump:
  - (a) Automatic air release valve as specified in 4-3.5.2,
  - (b) Water level detector as specified in 4-3.5.3,
  - (c) Discharge pressure gauge as specified in 2-5.1,
- (d) Relief valve and discharge cone where required by 2-13.1, and
- (e) Hose valve head and hose valves as specified in 2-14.3 or metering devices as specified in 2-14.2.
- 4-3.5.2 A 1½-in. (38.1 mm) pipe size or larger automatic air release valve shall be provided to vent air from the column and the discharge head upon the starting of the pump. This valve shall also admit air to the column to dissipate the vacuum upon stopping of the pump. It shall be located at the highest point in the discharge line between the fire pump and the discharge check valve.
- 4-3.5.3\* Each well installation shall be equipped with a suitable water level detector. If an air line is used it shall be corrosion-resistant metal, such as copper. Air lines shall be strapped to column pipe at 10-ft (3-m) intervals.

### 4-4\* Installation.

- **4-4.1 Pump House.** The pump house shall be of such design as will offer the least obstruction to the convenient handling and hoisting of vertical pump parts. The requirements of Sections 2-8 and 8-3 shall also apply.
- **4-4.2 Outdoor Setting.** If in special cases the authority having jurisdiction does not require a pump room and the unit is installed outdoors, the driver shall be screened or enclosed and adequately protected against tampering. The screen or enclosure shall be easily removable and shall have provision for ample ventilation.

### 4-4.3 Foundation.

**4-4.3.1** Certified dimension prints shall be obtained from the manufacturer.

- 4-4.3.2 The foundation for vertical pumps shall be substantially built to carry the entire weight of the pump and driver plus the weight of the water contained in it. Foundation bolts shall be provided to firmly anchor the pump to the foundation.
- **4-4.3.3** The foundation shall be of sufficient area and strength that the load per square inch on concrete does not exceed design standards.
- **4-4.3.4** The top of the foundation shall be carefully leveled to permit the pump to hang freely over a well pit on a short-coupled pump. On a well pump the pump head shall be positioned plumb over the well, which is not necessarily level.
- 4-4.3.5 Where the pump is mounted over a sump or pit, I beams shall be permitted to be used. Where a right-angle gear is used, the driver shall be installed parallel to the beams.

### 4.5 Driver.

### 4-5.1 Method of Drive.

4-5.1.1 The driver provided shall be so constructed that the total thrust of the pump (which includes the weight of the shaft, impellers, and hydraulic thrust) can be carried on a thrust bearing of ample capacity so that it will have an average life rating of 5-year continuous operation. All drivers shall be so constructed that axial adjustment of impellers can be made to permit proper installation and operation of the equipment. The pump shall be driven by a vertical hollow-shaft electric motor or vertical hollow-shaft right-angle gear drive with diesel engine or steam turbine.

Exception: Diesel engines and steam turbines designed and listed for vertical installation with vertical shaft turbine-type pumps are permitted to employ solid shafts and do not require a right-angle drive but do require a nonreverse ratchet.

**4-5.1.2** Motors shall be of the vertical hollow-shaft type, dripproof, normal starting torque, low starting current, squirrel cage induction type. The motor shall be equipped with a nonreverse ratchet.

### 4-5.1.3 Gear Drives.

4-5.1.3.1 Gear drives and flexible connecting shafts shall be acceptable to the authority having jurisdiction. They shall be of the vertical hollow-shaft type, permitting adjustment of the impellers for proper installation and operation of the equipment. The gear drive shall be equipped with a nonreverse ratchet.

- **4-5.1.3.2** All gear drives shall be listed and rated by the manufacturer at a load equal to the maximum horsepower and thrust of the pump for which the gear drive is intended.
- **4-5.1.3.3** Water-cooled gear drives shall be equipped with a visual means to determine if water circulation is occurring.
- **4-5.1.4** The flexible connecting shaft shall be listed for this service. The operating angle for the flexible connecting shaft shall not exceed the limits as required by the manufacturer for the speed and horsepower transmitted.
- **4-5.2 Controls.** The controllers for the motor, diesel engine, or steam turbine shall comply with specifications for either electric-drive controllers in Chapter 7 or engine-drive controllers in Chapter 9.
- 4-5.3 Each vertical shaft turbine-type fire pump shall have its own dedicated driver, and each driver shall have its own dedicated controller.

### 4-6 Tests.

### 4-6.1 Field Acceptance and Subsequent Tests.

- 4-6.1.1 When the installation is completed, an operating test shall be made in the presence of the customer, the pump manufacturer or its designated representative, and the authority having jurisdiction. Requirements in Section 11-2 shall be followed insofar as they apply, and for well installations the test also shall include a continuous run long enough to satisfy the authority having jurisdiction that the pump performs as required. In no event shall the test be for less than 1 hour.
- **4-6.1.2** At annual test time, both static and pumping water level shall be determined.

### 4-7 Operation and Maintenance.

### 4-7.1 Operation.

- 4-7.1.1\* Before the unit is started for the first time after installation, all field-installed electrical connections and discharge piping from the pump shall be checked. With the top drive coupling removed, the drive shaft shall be centered in the top drive coupling for proper alignment, and the motor shall be operated momentarily to ensure that it rotates in the proper direction. With the top drive coupling reinstalled, the impellers shall be set for proper clearance according to the manufacturer's instructions.
- **4-7.1.2\*** With the above precautions taken, the pump shall be started and allowed to run. The operation shall be observed for vibration while running, with vibration limits per *Hydraulics Institute Standards for Centrifugal, Rotary and Reciprocating Pumps*. The driver shall be observed for proper operation.

### 4-7.2 Maintenance.

- **4-7.2.1** The manufacturer's instructions shall be carefully followed in making repairs, dismantling, and reassembling pumps.
- 4-7.2.2 When spare or replacement parts are ordered, the pump serial number stamped on the nameplate fastened to the pump head shall be included in order to make sure the proper parts are provided.
- 4-7.2.3 Ample head room and access for removal of pump shall be maintained.

### Chapter 5 (Reserved)

### **Chapter 6** Electric Drive for Pumps

- 6-1 General. This chapter covers the minimum performance and testing requirements of the sources and transmission of electrical power to motors driving fire pumps and the minimum performance requirements of all intermediate equipment between the source(s) and the pump, including the motor(s), excepting the electric fire pump controller, transfer switch, and accessories (see Chapter 7). All electrical equipment and installation methods shall comply with NFPA 70, National Electrical Code, Article 695, and other applicable articles.
- **6-2 Power Source(s).** Power shall be supplied to the electric-motor-driven fire pump by one or more of the following, all of which shall make compliance with 6-3.1.2 possible.

Exception: Where electric motors are used and the height of the structure is beyond the pumping capability of the fire department apparatus, a reliable emergency source of power shall be provided for the pump installation.

- **6-2.1 Service.** Where power is supplied by a service, it shall be located and arranged to minimize the possibility of damage by fire from within the premises and exposing hazards.
- **6-2.2\* On-Site Generation.** Where power is supplied by on-site generation, the generation facility shall be located and protected to minimize the possibility of damage by fire.

### 6-2.3\* Other Sources.

- **6-2.3.1** For pump(s) driven by electric motor(s) where reliable power cannot be obtained from a private power station or utility service, one or more of the following shall also be provided:
  - (a) A secondary private power station or utility service,
  - (b) An on-site generator (see Section 6-2.4.2),
- (c) A redundant diesel-engine-driven fire pump complying with Chapter 8, or
- (d) A redundant steam-turbine-driven fire pump complying with Chapter 10.

## 6-2.4 Multiple Power Sources to Electric-Motor-Driven Fire Pumps.

- **6-2.4.1** Where multiple electric power sources are provided, they shall be arranged so that a fire at one source will not cause an interruption at the other source(s).
- **6-2.4.2 On-Site Generator.** Where alternate power is supplied by an on-site generator, the generator shall be located and protected in accordance with 6-2.1 and Section 6-6.
- 6-2.4.3 Supply conductors shall directly connect the power sources to either a listed combination fire pump controller and power transfer switch or to a disconnecting means and overcurrent protective device(s) meeting the requirements of 6-3.2.2, Exception No. 1.

Exception: Where one of the alternate power sources is an on-site generator, the disconnecting means and overcurrent protective device(s) for these supply conductors shall be selected or set to allow instantaneous pickup and running of the full pump room load.

### 6-3\* Power Supply Lines.

### 6-3.1 Circuit Conductors.

**6-3.1.1\*** Conductors feeding fire pump(s) and their accessories shall be dedicated and protected to resist possible damage by fire, structural failure, or operational accident.

6-3.1.2\* The voltage at the controller line terminals shall not drop more than 15 percent below normal (controller rated voltage) under motor starting conditions. The voltage at the motor terminals shall not drop more than 5 percent below the voltage rating of the motor when the motor is operating at 115 percent of the full-load current rating of the motor.

Exception: This starting limitation shall not apply for emergencyrun mechanical starting. (See 7-5.3.2.)

### 6-3.2 Power Supply Arrangement.

**6-3.2.1** The power supply to the fire pump shall not be disconnected when the plant power is disconnected.

6-3.2.2\* Power Supply Arrangements from Normal Source to Pump Motor. The supply conductors shall directly connect the power source to a listed fire pump controller.

Exception No. 1: A disconnecting means and overcurrent protective device(s) shall be permitted to be installed between the power supply and the listed fire pump controller if installed remotely from the other service(s) disconnecting means. The disconnecting means and the overcurrent protective device(s) shall comply with the following:

- (a) The overcurrent protective device(s) shall be selected or set to carry indefinitely the sum of the locked rotor current of the fire pump motor(s) and the pressure maintenance pump motor(s) and the full load current of the associated fire pump accessory equipment when connected to this power supply.
- (b) The disconnecting means shall be marked suitable for use as service equipment and shall be lockable in the "ON" position.
- (c) A placard shall be externally installed on the disconnecting means stating "Fire Pump Disconnecting Means." The letters shall be at least 1 in. (25.4 mm) in height.
- (d) A placard shall be placed adjacent to the fire pump controller stating the location of this disconnecting means and the location of the key (if the disconnecting means is locked).
- (e) The disconnecting means shall be supervised in the closed position by one of the following methods:
- 1. Central station, proprietary, or remote station signal device;
- 2. Local signaling service that will cause the sounding of an audible signal at a constantly attended location;
  - 3. Locking the disconnecting means closed; or
- 4. Sealing of the disconnecting means and approved weekly recorded inspections where the disconnecting means are located within fenced enclosures or in buildings under the control of the owner.

Exception No. 2: Where the supply voltage is different from the utilization voltage of the fire pump motor, a transformer meeting the requirements of Section 695-5 of NFPA 70, National Electrical Code, and a disconnecting means and overcurrent protective device(s) meeting the requirements of Exception No. 1 shall be installed.

### 6-4 Motors.

### 6-4.1 General.

6-4.1.1 All motors shall be specifically listed for fire pump service. (This requirement shall be effective January 1, 1998.)

Table 6-4.1.1 Horsepower and Locked Rotor Current Motor
Designation

Rated Horsepower	Locked Rotor Current Three-Phase 460 Volts (Amps)	Motor Designation (NEC, Locked Rotor Indicating Code Letter) "A" to and Including		
5	46	J		
7 1/2	64	Й		
10	81	Н		
15	116	G		
20	145	G		
25	183	G		
30	217	G		
40	290	G		
50	362	G		
60	435	G		
75	543	G		
100	725	G		
125	908	G		
150	1085	G		
200	1450	G		
250	1825	G		
300	2200	G		
350	2550	G		
400	2900	G		
450	3250	G		
500	3625	G		

NOTE: The locked rotor currents for 460-volt motors are approximately 6 'times the full load current. The corresponding values of locked rotor current for motors rated at other voltages shall be determined by multiplying the values shown by the ratio of 460 volts to the rated voltage.

Code letters of motors for all other voltages shall conform with those shown for 460 volts.

- **6-4.1.2** All motors shall comply with NEMA Standard MG-1 and shall be marked as complying with NEMA Design B standards.
- [6-4.1.3 All motors shall be rated for continuous duty.
- **6-4.1.4** Electric-motor-induced transients shall be coordinated with the provisions of 7-4.3.3 to prevent nuisance tripping of motor controller protective devices.

### 6-4.2 Current Limits.

6-4.2.1 The motor capacity in horsepower shall be such that the maximum motor current in any phase under any condition of pump load and voltage unbalance shall not exceed the motor-rated full-load current multiplied by the service factor. The maximum service factor at which a motor can be used is 1.15. These service factors shall be in accordance with NEMA Standard MG-1.

Exception: General-purpose (open and dripproof) motors, totally enclosed fan-cooled (TEFC) motors, and totally enclosed nonventilated (TENV) motors shall not have a service factor larger than 1.15.

**6-4.2.2** Motors used at altitudes above 3300 ft (1000 m) shall be operated or derated according to NEMA Standard MG-1, Part 14.

### 6-4.3 Marking.

- 6-4.3.1 Marking of motor terminals shall be in accordance with NEMA Standard MG-1, Part 2.
- **6-4.3.2** A motor terminal connecting diagram for multiple lead motors shall be furnished by the motor manufacturer.

### 6-5 Motor Application.

- **6-5.1** Where unusual moisture or abrasive dust conditions are anticipated, motors shall be a special type or specially insulated to withstand such conditions.
- **6-5.2** Where subject to possible splash of water, motors shall be totally enclosed.
- **6-5.3** Totally enclosed motors shall have conduit terminations arranged to prevent the entrance of water.

### 6-6 On-Site Power Generator Systems.

- 6-6.1 Where on-site generator systems are used to supply power to fire pump motors to meet the requirements of 6-2.3.1, they shall be of sufficient capacity to allow normal starting and running of the motor(s) driving the fire pump(s) while supplying all other loads connected to the generator.
- **6-6.2** Automatic shedding of loads not required for fire protection shall be permitted immediately prior to starting of the fire pump(s). This load shedding shall not increase the delay in starting of the fire pump(s) by more than 10 seconds.
- 6-6.3\* These power sources shall comply with 6-3.1.2 and shall meet the requirements of Level 1, Type 10, Class X systems of NFPA 110, Standard for Emergency and Standby Power Systems. The fuel supply capacity shall be sufficient to provide 8 hours of fire pump operation at 100 percent of the rated pump capacity in addition to the supply required for other demands.
- **6-6.4** Automatic sequencing of the fire pumps shall be permitted in accordance with **7-5.2.4**.
- **6-6.5** Transfer of power shall take place within the pump room.
- 6-6.6 Protective devices in the on-site power source circuits at the generator shall allow instantaneous pickup of the full pump room load.

# Chapter 7 Electric Drive Controllers and Accessories

7-1 Application. This chapter covers the minimum performance and testing requirements for controllers and transfer switches for electric motors driving fire pumps. Accessory devices, including alarm monitoring and signaling means, are included where necessary to ensure the minimum performance of the aforementioned equipment.

### 7-1.1 General.

- **7-1.1.1** All controllers shall be specifically listed for electric-motor-driven fire pump service.
- 7-1.1.2\* The controller and transfer switch shall be suitable for the available short-circuit current at the line termi-

nals of the controller and transfer switch and shall be marked "Suitable for Use on a Circuit Capable of Delivering Not More than Amperes RMS Symmetrical at Volts AC."

- NOTE: The blank spaces shown shall have appropriate numbers filled in for each installation.
- **7-1.1.3** All controllers shall be completely assembled, wired, and tested by the manufacturer before shipment from the factory.
- **7-1.1.4** All controllers shall be listed as suitable for use as service equipment where so used.
- 7-1.1.5 All controllers shall be marked "Electric Fire Pump Controller" and shall show plainly the name of the manufacturer, the identifying designation, and the complete electrical rating. Where multiple pumps are provided, one or more serving different areas or portions of the facility, an appropriate sign shall be conspicuously attached to each controller indicating the area, zone, or portion of the system served by that pump or pump controller.
- 7-1.1.6 It shall be the responsibility of the pump manufacturer or its designated representative to make necessary arrangements for the services of a manufacturer's representative when needed for service and adjustment of the equipment during the installation, testing, and warranty periods.

### 7-2 Location.

- 7-2.1\* Controllers shall be located as close as is practical to the motors they control and shall be within sight of the motors.
- 7-2.2 Controllers shall be so located or so protected that they will not be injured by water escaping from pumps or pump connections. Current-carrying parts of controllers shall be not less than 12 in. (305 mm) above the floor level.
- **7-2.3** Working clearances around controllers shall comply with NFPA 70, *National Electrical Code*, Article 110.

### 7-3 Construction.

- **7-3.1 Equipment.** All equipment shall be suitable for use in locations subject to a moderate degree of moisture, such as a damp basement.
- **7-3.2 Mounting.** All equipment shall be mounted in a substantial manner on a single noncombustible supporting structure.

### 7-3.3 Enclosures.

- 7-3.3.1 The structure or panel shall be securely mounted in a NEMA Type 2, dripproof, as a minimum, enclosure(s). (See NEMA Standard 250, Enclosures for Electrical Equipment.) Where the equipment is located outside or special environments exist, suitably rated enclosures shall be used.
- **7-3.3.2** Grounding. The enclosure(s) shall be grounded in accordance with NFPA 70, *National Electrical Code*, Article 250.

### 7-3.4 Connections and Wiring.

7-3.4.1 All busbars and connections shall be readily accessible for maintenance work after installation of the controller. These connections shall be arranged so that disconnection of the external circuit conductors will not be required.

- **7-3.4.2 Test Provisions.** Provisions shall be made within the controller to permit the use of test instruments for measuring all line voltages and currents without disconnecting any conductors within the controller.
- **7-3.4.3** Busbars and other wiring elements of the controller shall be designed on a continuous-duty basis.

Exception: Conductors that are in a circuit only during the motor starting period shall be permitted to be designed accordingly.

- **7-3.4.4** A fire pump controller shall not be used as a junction box to supply other equipment. Electrical supply conductors for pressure maintenance (jockey or make-up) pump(s) shall not be connected to the fire pump controller.
- 7-3.5 Protection of Auxiliary Circuits. Circuits that are necessary for proper operation of the controller shall not have overcurrent protective devices connected in them.
- **7-3.6 External Operation.** All switching equipment for manual use in connecting or disconnecting, or starting or stopping, the motor shall be externally operable. (See NFPA 70, National Electrical Code.)

### 7-3.7 Electrical Diagrams and Instructions.

- **7-3.7.1** An electrical schematic diagram shall be provided and permanently attached to the inside of the controller enclosure.
- 7-3.7.2 All the field wiring terminals shall be plainly marked to correspond with the field connection diagram furnished.
- 7-3.7.3\* Complete instructions covering the operation of the controller shall be provided and conspicuously mounted on the controller.
- 7-3.8 Marking. Each motor control device and each switch and circuit breaker shall be marked to plainly indicate the name of the manufacturer, the designated identifying number, and the electrical rating in volts, horsepower, amperes, frequency, phases, etc., as appropriate. The markings shall be so located as to be visible after installation.

### 7-4 Components.

7-4.1\* Voltage Surge Arrester. A voltage surge arrester complying with ANSI/IEEE C62.1 or C62.11 shall be installed from each phase to ground. (See 7-3.2.) The surge arrester shall be rated to suppress voltage surges above line voltage.

Exception No. 1: These voltage surge arresters shall not be mandatory for controllers rated in excess of 600 volts. (See Section 7-6.) Exception No. 2: These voltage surge arresters shall not be mandatory if the controller can withstand without damage a 10-kV impulse in accordance with ANSI/IEEE C62.41.

### 7-4.2 Isolating Switch.

**7-4.2.1** The isolating switch shall be a manually operable motor circuit switch or a molded case switch having a horse-power rating equal to or greater than the motor horsepower.

Exception No. 1: A molded case switch having an ampere rating not less than 115 percent of the motor rated full load current (see NFPA 70, National Electrical Code) and also suitable for interrupting the motor locked rotor current shall be permitted.

- Exception No. 2: A molded case isolating switch shall be permitted to have self-protecting instantaneous short-circuit overcurrent protection, provided that this switch does not trip unless the circuit breaker in the same controller trips.
- 7-4.2.2 The isolating switch shall be externally operable.
- 7-4.2.3 The ampere rating of the isolating switch shall be at | least 115 percent of the full-load current rating of the motor. (See NFPA 70, National Electrical Code.)
- **7-4.2.4** The following warning shall appear on or immediately adjacent to the isolating switch:

# WARNING — DO NOT OPEN OR CLOSE THIS SWITCH WHILE THE CIRCUIT BREAKER (DISCONNECTING MEANS) IS IN CLOSED POSITION.

Exception: Where the isolating switch and the circuit breaker are so interlocked that the isolating switch can neither be opened nor closed while the circuit breaker is closed, the warning label shall be permitted to be replaced with an instruction label that directs the order of operation. This label shall be permitted to be part of the label required by 7-3.7.3.

7-4.2.5 The isolating switch operating handle shall be provided with a spring latch that shall be so arranged that it requires the use of the other hand to hold the latch released in order to permit opening or closing of the switch.

Exception: Where the isolating switch and the circuit breaker are so interlocked that the isolating switch can neither be opened nor closed while the circuit breaker is closed, this latch shall not be required.

### 7-4.3 Circuit Breaker (Disconnecting Means).

7-4.3.1 The motor branch circuit shall be protected by a circuit breaker (see NFPA 70, National Electrical Code, Article 100) that shall be connected directly to the load side of the isolating switch and shall have one pole for each ungrounded circuit conductor.

Exception: Where the motor branch circuit is transferred to an alternate on-site power generator and is protected by an overcurrent device at the generator (see 6-6.6), the circuit breaker within the fire pump controller shall be permitted to be bypassed when that motor branch circuit is so connected.

- 7-4.3.2 The circuit breaker shall have the following mechanical characteristics:
  - (a) It shall be externally operable (see 7-3.6).
  - (b) It shall trip free of the handle.
- (c) A nameplate with the legend "CIRCUIT BREAKER DISCONNECTING MEANS" in letters not less than  $\Re_8$  in. (10 mm) high shall be located on the outside of the controller enclosure adjacent to the means for operating the circuit breaker.
- 7-4.3.3\* The circuit breaker shall have the following electrical characteristics:
- (a) A continuous current rating not less than 115 percent of the rated full load current of the motor;
  - (b) Overcurrent sensing elements of the nonthermal type;
  - (c) Instantaneous short-circuit overcurrent protection;
- (d)\* An adequate interrupting rating to provide the suitability rating (see 7-1.1.2) of the controller;

- (e) Capability of allowing normal and emergency (see 7-5.3.2) starting and running of the motor without tripping; and
- (f) An instantaneous trip setting of not more than 20 times the full load current.

Exception:\* Current limiters, where integral parts of the circuit breaker, shall be permitted to be used to obtain the required interrupting rating, provided all of the following requirements are met:

- 1. The breaker shall accept current limiters of only one rating.
- 2. The current limiters shall hold 300 percent of full load motor current for a minimum of 30 minutes.
- 3. The current limiters, where installed in the breaker, shall not open at locked rotor current.
- 4. A spare set of current limiters of correct rating shall be kept readily available in a compartment or rack within the controller enclosure.
- **7-4.4 Locked Rotor Overcurrent Protection.** The only other overcurrent protective device that shall be required and permitted between the isolating switch and the fire pump motor shall be located within the fire pump controller and shall possess the following characteristics:
- (a) For a squirrel-cage or wound-rotor induction motor, the device shall be:
- 1. Of the time-delay type having a tripping time between 8 seconds and 20 seconds at locked rotor current (approximately 600 percent of rated full load current for a squirrel-cage induction motor); and
- 2. Calibrated and set at a minimum of 300 percent of motor full load current.
  - (b) For a direct-current motor, the device shall be:
    - 1. Of the instantaneous type; and
- 2. Calibrated and set at a minimum of 400 percent of motor full load current.
- (c) There shall be visual means or markings clearly indicated on the device that proper settings have been made.
- (d) It shall be possible to reset the device for operation immediately after tripping, with the tripping characteristics thereafter remaining unchanged.
- (e) Tripping shall be accomplished by opening the circuit breaker, which shall be of the external manual reset type.

### 7-4.5 Motor Contactor.

- | 7-4.5.1 The motor contactor shall be horsepower rated and shall be of the magnetic type with a contact in each ungrounded conductor.
- **7-4.5.2** For electrical operation of reduced-voltage controllers, timed automatic acceleration of the motor shall be provided. The period of motor acceleration shall not exceed 10 seconds.
- **7-4.5.3** Starting resistors shall be designed to permit one 5-second starting operation every 80 seconds for a period of not less than 1 hour.
- **7-4.5.4** Starting reactors and autotransformers shall be designed to permit one 15-second starting operation every 240 seconds for a period of not less than 1 hour.

Exception: Designs in accordance with the requirements of NEMA Industrial Control and Systems Standards (Part ICS 2.2) for medium-duty service shall be acceptable for controllers over 200 hp.

- 7-4.5.5 The operating coil for the main contactor shall be supplied directly from the main power voltage and not through a transformer (for controllers of 600 volts or less).
- **7-4.5.6** No undervoltage, phase-loss, frequency-sensitive, or other sensor(s) shall be installed that automatically or manually prohibit actuation of the motor contactor.

### 7-4.6\* Alarm and Signal Devices on Controller.

7-4.6.1 Power Available Visible Indicator. A visible indicator shall be connected to a pair of power supply conductors directly on the line terminals of the motor contactor. This visible indicator shall demonstrate that operating voltage is available to the contactor coil. If the visible indicator is a pilot lamp, it shall be accessible for replacement.

Exception: When power is supplied from multiple power sources, monitoring of each power source for phase loss shall be permitted at any point electrically upstream of the line terminals of the contactor provided all sources are monitored.

**7-4.6.2 Phase Reversal.** Phase reversal of the power source to which the line terminals of the motor contactor are connected shall be indicated by a visible indicator.

Exception: When power is supplied from multiple power sources, monitoring of each power source for phase reversal shall be permitted at any point electrically upstream of the line terminals of the contactor provided all sources are monitored.

- 7-4.7 Alarm and Signal Devices Remote from Controller. Where the pump room is not constantly attended, audible or visual alarms powered by a source not exceeding 125 volts shall be provided at a point of constant attendance. These alarms shall indicate the following:
- (a) Controller has operated into a motor running condition. This alarm circuit shall be energized by a separate reliable supervised power source, or from the pump motor power, reduced to not more than 125 volts.
- (b)\* Loss of any phase at the line terminals of the motor contactor. (All phases shall be monitored.)

Exception: When power is supplied from multiple power sources, monitoring of each power source for phase loss shall be permitted at any point electrically upstream of the line terminals of the contactor provided all sources are monitored.

- (c) Phase Reversal (see 7-4.6.2). This alarm circuit shall be energized by a separate reliable supervised power source, or from the pump motor power, reduced to not more than 125 volts.
- (d) Connections to Alternate Source. Where two sources of power are supplied to meet the requirements of 6-2.3.1, this alarm circuit shall be energized by a separate reliable supervised power source, reduced to not more than 125 volts.
- 7-4.8 Controller Alarm Contacts for Remote Indication. Controllers shall be equipped with contacts (open or closed) to operate circuits for the conditions covered in 7-4.7.

### 7-5 Starting and Control.

### 7-5.1\* Automatic and Nonautomatic.

- **7-5.1.1** An automatic controller shall be operable also as a nonautomatic controller.
- **7-5.1.2** A nonautomatic controller shall be actuated by manually initiated electrical means and by manually initiated mechanical means.

### 7-5.2 Automatic Controller.

- 7-5.2.1\* Water Pressure Control. There shall be provided a pressure-actuated switch having independent high-and low-calibrated adjustments in the controller circuit. There shall be no pressure snubber or restrictive orifice employed within the pressure switch. This switch shall be responsive to water pressure in the fire protection system. The pressure sensing element of the switch shall be capable of withstanding a momentary surge pressure of 400 psi (27.6 bars) without losing its accuracy. Suitable provision shall be made for relieving pressure to the pressure-actuated switch to allow testing of the operation of the controller and the pumping unit. [See Figures A-7-5.2.1(a) and (b).]
- (a) For all pump installations (including jockey pumps) each controller shall have its own individual pressure sensing line.
- (b) The pressure sensing line connection for each pump (including jockey pumps) shall be made between that pump's discharge check valve and discharge control valve. This line shall be corrosion-resistant metallic pipe or tube, and the fittings (brass, copper, or series 300 stainless steel) shall be of ½-in. (12.7-mm) nominal size. There shall be two check valves installed in the pressure sensing line at least 5 ft (1.5 m) apart with a 3/32-in. (2.4-mm) hole drilled in the clapper to serve as dampening. [See Figures A-7-5.2.1(a) and (b) for clarification.]

Exception: If water is clean, ground-face unions with noncorrosive diaphragms drilled with  $\frac{3}{32}$ -in. (2.4-mm) orifices shall be permitted in place of the check values.

- (c) There shall be no shutoff valve in the pressure sensing line.
- (d) Pressure switch actuation at the low adjustment setting shall initiate pump starting sequence (if pump is not already in operation).
- 7-5.2.2 Fire Protection Equipment Control. Where the pump supplies special water control equipment (deluge valves, dry pipe valves, etc.), it may be desirable to start the motor before the pressure-actuated switch(es) would do so. Under such conditions the controller shall be equipped to start the motor upon operation of the fire protection equipment. Starting of the motor shall be initiated by the opening of a normally closed contact on the fire protection equipment.
- **7-5.2.3** Manual Electric Control at Remote Station. Where additional control stations for causing nonautomatic continuous operation of the pumping unit, independent of the pressure-actuated switch, are provided at locations remote from the controller, such stations shall not be operable to stop the motor.
- 7-5.2.4 Sequence Starting of Pumps. The controller for each unit of multiple pump units shall incorporate a sequential timing device to prevent any one motor from starting simultaneously with any other motor. Each pump supplying suction pressure to another pump shall be arranged to start before the pump it supplies. If water requirements call for more than one pumping unit to operate, the units shall start at intervals of 5 to 10 seconds. Failure of a leading motor to start shall not prevent subsequent pumping units from starting.
- **7-5.2.5 External Circuits Connected to Controllers.** External control circuits shall be arranged so that failure of any external circuit (open or short circuit) shall not prevent

operation of pump(s) from all other internal or external means. Breakage, disconnecting, shorting of the wires, or loss of power to these circuits can cause continuous running of the fire pump but shall not prevent the controller(s) from starting the fire pump(s) due to causes other than these external circuits.

**7-5.2.6 Pressure Recorder.** An automatic controller shall be equipped with a pressure-recording device that shall operate continuously for at least 7 days without resetting or rewinding.

### 7-5.3 Nonautomatic Controller.

7-5.3.1 Manual Electric Control at Controller. There shall be a manually operated switch on the control panel so arranged that, when the motor is started manually, its operation cannot be affected by the pressure-actuated switch. The arrangement shall also provide that the unit will remain in operation until manually shut down.

### 7-5.3.2 Emergency Run Mechanical Control at Controller.

- (a) The controller shall be equipped with an emergency run handle or lever that operates to mechanically close the motor-circuit switching mechanism. This handle or lever shall provide for nonautomatic continuous running operation of the motor(s), independent of any electric control circuits, magnets, or equivalent devices and independent of the pressure-activated control switch. Means shall be incorporated for mechanically latching or holding the handle or lever for manual operation in the actuated position. The mechanical latching shall not be automatic, but at the option of the operator.
- (b) The handle or lever shall be arranged to move in one direction only from "off" to final position.
- (c) The motor starter shall return automatically to the "off" position in case the operator releases the starter handle or lever in any position but the full running position.
- **7-5.4 Methods of Stopping.** Shutdown shall be accomplished by the following methods:
- (a) Manual. Operation of a pushbutton on the outside of the controller enclosure that, in the case of automatic controllers, shall return the controller to full automatic position.
- (b) Automatic Shutdown after Automatic Start (Optional). If the controller is arranged for automatic shutdown after starting causes have returned to normal, a running period timer set for at least 10 minutes running time shall be used.

Exception: Automatic shutdown shall not be permitted where the pump constitutes the sole supply of a fire sprinkler or standpipe system or where the authority having jurisdiction has required manual shutdown.

### 7-6 Controllers Rated in Excess of 600 Volts.

- 7-6.1\* Control Equipment. Controllers rated in excess of 600 volts shall comply with the requirements of this chapter, except as provided in 7-6.2 through 7-6.8.
- 7-6.2 Provisions for Testing. The provisions of 7-3.4.2 shall not apply. An ammeter shall be provided on the controller with a suitable transfer switch arranged for reading the current in each phase. An indicating voltmeter, deriving its source of power of not more than 125 volts from a transformer(s) connected to the high-voltage supply, shall also be provided with a suitable selector switch arranged for reading each phase voltage.

### 7-6.3 Disconnecting Under Load.

- **7-6.3.1** Provisions shall be made to prevent the isolating switch from being opened under load.
- **7-6.3.2** A load-break disconnecting means shall be permitted to be used in lieu of the isolating switch if the fault closing and interrupting ratings equal or exceed the requirements of the installation.
- 7-6.4 Pressure-Actuated Switch Location. Special precautions shall be taken in locating the pressure-actuated switch called for in 7-5.2.1 to prevent any water leakage from coming in contact with high-voltage components.
- 7-6.5 Low-Voltage Control Circuit. The low-voltage control circuit shall be supplied from the high-voltage source through a step-down transformer(s) protected by high-voltage fuses in each primary line. Its power supply shall be interrupted when the isolating switch is in the open position. The secondary of the transformer and control circuitry shall otherwise comply with 7-3.5. One secondary line shall be grounded unless all control and operator devices are rated for use at the high (primary) voltage.
- 7-6.6 Alarm and Signal Devices on Controller. Specifications for controllers rated in excess of 600 volts differ from those in 7-4.6. A visible indicator shall be provided to indicate that power is available. The current supply for the visible indicator shall come from the secondary of the control circuit transformer through resistors, if found necessary, or from a small-capacity step-down transformer, which shall reduce the control transformer secondary voltage to that required for the visible indicator. If the visible indicator is a pilot lamp, it shall be accessible for replacement.
- **7-6.7 Protection of Personnel from High Voltage.** Necessary provisions shall be made, including such interlocks as may be needed, to protect personnel from accidental contact with high voltage.
- 7-6.8 Disconnecting Means. A contactor in combination with current-limiting motor circuit fuses shall be permitted to be used in lieu of the circuit breaker (disconnecting means) required in 7-4.3.1 if all of the following requirements are met.
- (a) Current-limiting motor circuit fuses shall be mounted in the enclosure between the isolating switch and the contactor. They shall interrupt the short-circuit current available at the controller input terminals.
- (b) These fuses shall have an adequate interrupting rating to provide the suitability rating (see 7-1.1.2) of the controller.
- (c) The current-limiting fuses shall be sized to hold 600 percent of the full-load current rating of the motor for at least 100 seconds.
- (d) A spare set of fuses of the correct rating shall be kept readily available in a compartment or rack within the controller enclosure.
- 7-6.9 Locked Rotor Overcurrent Protection. Tripping of the locked rotor overcurrent device required by 7-4.4 shall be permitted to be accomplished by opening the motor contactor coil circuit(s) to drop out the contactor. Means shall be provided to restore the controller to normal operation by an external manually reset device.

- 7-6.10 Emergency Run Mechanical Control at Controller. The controller shall comply with 7-5.3.2(a) and (b) except the mechanical latching may be automatic. When the contactor is latched-in, the locked rotor over current protection of 7-4.4 is not required.
- 7-7\* Limited Service Controllers. Limited service controllers consisting of automatic controllers for across-the-line starting of squirrel-cage motors of 30 hp or less, 600 volts or less, shall be permitted to be installed where such use is acceptable to the authority having jurisdiction. The provisions of Sections 7-1 through 7-5 shall apply.
- Exception No. 1: In lieu of 7-4.3.3(b) and 7-4.4, the locked rotor overcurrent protection shall be permitted to be achieved by using an inverse time nonadjustable circuit breaker having a standard rating between 150 percent and 250 percent of the motor full-load current.
- Exception No. 2: Each controller shall be marked "Limited Service Controller" and shall show plainly the name of the manufacturer, the identifying designation, and the complete electrical rating. (See 7-4.2.1.)
- Exception No. 3: The controller shall have a short-circuit current rating not less than 10,000 amps.

Exception No. 4: The manually operated isolating switch specified in 7-4.2 shall not be required.

### 7-8\* Power Transfer for Alternate Power Supply.

### 7-8.1 General.

- **7-8.1.1** Where required by the authority having jurisdiction or to meet the requirements of 6-2.3.1 where an on-site electrical power transfer device is used for power source selection, such switch shall comply with the provisions of this paragraph as well as Sections 7-1, 7-2, 7-3, and 7-4.1.
- **7-8.1.2** Manual transfer switches shall not be used to transfer power between the normal supply and the alternate supply to the fire pump controller.
- **7-8.1.3** No remote device(s) shall be installed that will prevent automatic operation of the transfer switch.
- 7-8.2\* Fire Pump Controller and Transfer Switch Arrangements.
- 7-8.2.1 Arrangement I (Listed Combination Fire Pump Controller and Power Transfer Switch).
- 7-8.2.1.1 Where the power transfer switch consists of a self-contained power switching assembly, such assembly shall be housed in a barriered compartment of the fire pump controller or in a separate enclosure attached to the controller and marked "Fire Pump Power Transfer Switch."
- **7-8.2.1.2** An isolating switch, complying with 7-4.2, located within the power transfer switch enclosure or compartment shall be provided ahead of the alternate input terminals of the transfer switch.
- (a) The isolating switch shall be supervised to indicate when it is open.
- (b) Supervision shall operate an audible and visual signal in the pump room and at a remote point when required.
- (c) The isolating switch shall be suitable for the available short-circuit current of the alternate source.
- **7-8.2.1.3** Where the alternate source is provided by a second utility power source, the transfer switch emergency side shall be provided with an isolation switch complying with 7-4.2 and a circuit breaker complying with 7-4.3 and 7-4.4.

- 7-8.2.2 Arrangement II (Individually Listed Fire Pump Controller and Power Transfer Switch). The following shall be provided:
- (a) A fire pump controller power transfer switch complying with Sections 6-6 and 7-8 and a fire pump controller.
- (b) An isolating switch (or service disconnect where required) ahead of the normal input terminals of the transfer switch.
- (c) Where the alternate source is supplied by a second utility, the transfer switch overcurrent protection shall be selected or set to indefinitely carry the locked rotor current of the fire pump motor.
- (d) An isolating switch ahead of the alternate source input terminals of the transfer switch and meeting the following requirements:
- 1. The isolating switch shall be lockable in the "on" position.
- 2. A placard shall be externally installed on the isolating switch stating "Fire Pump Isolating Switch." The letters shall be at least 1 in. (25.4 mm) in height.
- 3. A placard shall be placed adjacent to the fire pump controller stating the location of this switch and the location of the key (if the isolating switch is locked.)
- 4. The isolating switch shall be supervised to indicate when it is not closed by one of the following methods:
- a. Central station, proprietary, or remote station signal service;
- b. Local signaling service that will cause the sounding of an audible signal at a constantly attended point;
  - c. Locking the isolating switch closed; or
- d. Sealing of isolating switches and approved weekly recorded inspections where isolating switches are located within fenced enclosures or in buildings under the control of the owner.
- **7-8.2.3** Each fire pump shall have its own dedicated transfer switch(es) where a transfer switch(es) is required.
- 7-8.2.4 The fire pump controller and transfer switch (see 7-8.2.1 and 7-8.2.2) shall each have a cautionary marking to indicate that the isolation switch for both the controller and transfer switch is opened before servicing the controller, transfer switch, or motor.

### 7-8.3 Power Transfer Switch Requirements.

- **7-8.3.1** The power transfer switch shall be specifically listed for fire pump service.
- 7-8.3.2 The power transfer switch shall be suitable for the available short-circuit currents at the transfer switch normal and alternate input terminals.
- **7-8.3.3** The power transfer switch shall be electrically operated and mechanically held.
- 7-8.3.4 The power transfer switch shall have a horsepower rating at least equal to the motor horsepower or, where rated in amperes, shall have an ampere rating not less than 115 percent of the motor full-load current and also suitable for switching the motor locked rotor current.
- **7-8.3.5** A means for safe manual (nonelectrical) operation of the power transfer switch shall be provided. This manual means need not be externally operable.

7-8.3.6 The power transfer switch shall be provided with undervoltage sensing devices to monitor all ungrounded lines of the normal power source. Where the voltage on any phase at the load terminals of the circuit breaker within the fire pump controller falls below 85 percent of motor rated voltage, the power transfer switch shall automatically initiate transfer to the alternate source. Where the voltage on all phases of the normal source returns to within acceptable limits, the fire pump controller shall be permitted to be retransferred to the normal source. Phase reversal of the normal source power (see 7-4.6.2) shall cause a simulated normal source power failure upon sensing phase reversal.

Exception: Where the power transfer switch is electrically upstream of the fire pump controller circuit breaker, voltage shall be permitted to be sensed at the input to the power transfer switch in lieu of at the load terminals of the fire pump controller circuit breaker.

7-8.3.7 Voltage- and frequency-sensing devices shall be provided to monitor at least one ungrounded conductor of the alternate power source. Transfer to the alternate source shall be inhibited until there is adequate voltage and frequency to serve the fire pump load.

Exception: Where the alternate source is provided by a second utility power source, undervoltage sensing devices shall monitor all ungrounded conductors in lieu of a frequency-sensing device.

- **7-8.3.8** Two visible indicators shall be provided to externally indicate the power source to which the fire pump controller is connected.
- **7-8.3.9** Means shall be provided to delay retransfer from the alternate source of power to the normal source until the normal source is stabilized. This time delay shall be automatically bypassed if the alternate source fails.
- '7-8.3.10 Means shall be provided to prevent higher-thannormal inrush currents when transferring the fire pump motor from one source to the other.
- **7-8.3.11** The power transfer switch shall not have integral short-circuit or overcurrent protection.

### 7-8.3.12 The following shall be provided:

- (a) A device to delay starting of the alternate source generator to prevent nuisance starting in the event of momentary dips and interruptions of the normal source;
- (b) A circuit loop to the alternate source generator whereby either the opening or closing of the circuit will start the alternate source generator (when commanded by the power transfer switch) (see 7-8.3.6); and
- (c) A means to prevent sending of the signal for starting of the alternate source generator when commanded by the power transfer switch, if the isolation switch on the alternate source side of the transfer switch is open.
- **7-8.3.13** A momentary test switch, externally operable, shall be provided on the enclosure that will simulate a normal power source failure.
- **7-8.3.14** Auxiliary contacts (open or closed) mechanically operated by the fire pump power transfer switch mechanism shall be provided for remote indication that the fire pump controller has been transferred to the alternate source.

- 7-9 Controllers for Foam Concentrate Pump Motors.
- **7-9.1 Control Equipment.** Controllers for foam concentrate pump motors shall comply with the requirements of Sections 7-1 through 7-5 of this chapter except as provided in 7-9.2 through 7-9.5.
- **7-9.2 Automatic Starting.** In lieu of the pressure-actuated switch described in 7-5.2.1, automatic starting shall be capable of being accomplished by the automatic activation of either a remote normally open contact or a remote normally closed contact.
- 7-9.3 Methods of Stopping. The run period timer described in 7-5.4(b), if required, shall be set to less than 10 minutes but not less than 1 minute in controllers used in foam service.
- **7-9.4 Lockout.** Where required, the controller shall contain a lockout feature to stop the foam concentrate pump motor on loss of foam concentrate or when used in a duty-standby application. Where supplied, this lockout shall be indicated by a visible indicator and provisions for annunciating the condition at a remote location.
- **7-9.5 Marking.** The controller shall be marked "Foam Pump Controller."

### Chapter 8 Diesel Engine Drive

### 8-1 General.

- **8-1.1 Selection.** Selection of diesel-engine-driven fire pump equipment for each situation shall be based on careful consideration of the following factors: most reliable type of control, fuel supply, installation, and the starting and running operation of the diesel engine.
- 8-1.2 Experience Record. The compression ignition diesel engine has proved to be the most dependable of the internal combustion engines for driving fire pumps. Except for installations made prior to adoption of the 1974 edition of this standard, spark-ignited internal combustion engines shall not be used. This restriction shall not be interpreted to exclude gas turbine engines as future pump drivers.

### 8-2 Engines.

- 1 8-2.1 Listing. Engines shall be listed for fire pump service.
- **8-2.1.1** Engines shall be specifically listed for fire pump service by a testing laboratory.

### 8-2.2 Engine Ratings.

- **8-2.2.1** Engines shall be rated at standard SAE conditions of 29.61 in. (752.1 mm) Hg barometer and 77°F (25°C) inlet air temperature [approximates 300 ft (91.4 m) above sea level] by the testing laboratory. (See SAE Standard J-1349, Engine Power Test Code Spark Ignition and Compression Engine.)
- **8-2.2.2** Engines shall be acceptable for horsepower ratings listed by the testing laboratory for standard SAE conditions.
- **8-2.2.3** In special cases, engines outside the power range and type of listed engines shall have a horsepower capability, where equipped for fire pump driver service, not less than 10 percent greater than the maximum brake horsepower required by the pump under any conditions of pump load. The engine shall meet all the other requirements of listed engines.

- **8-2.2.4\*** A deduction of 3 percent from engine horsepower rating at standard SAE conditions shall be made for diesel engines for each 1000 ft (305 m) of altitude above 300 ft (91.4 m).
- 8-2.2.5\* A deduction of 1 percent from engine horsepower rating as corrected to standard SAE conditions shall be made for diesel engines for every 10°F (5.6°C) above 77°F (25°C) ambient temperature.
- **8-2.2.6** Where right-angle gear drives (see 8-2.3.2) are used between the vertical turbine pump and its driver, the horse-power requirement of the pump shall be increased to allow for power loss in the gear drive.
- 8-2.2.7 After complying with the requirements of 8-2.2.1 through 8-2.2.6, engines shall have a 4-hr minimum horse-power rating equal to or greater than the brake horsepower required to drive the pump at its rated speed under any conditions of pump load.

### 8-2.3 Engine Connection to Pump.

- 8-2.3.1 Horizontal Shaft Pumps. Engines shall be connected to horizontal shaft pumps by means of a flexible coupling or flexible connecting shaft listed for this service. The flexible coupling shall be directly attached to the engine flywheel adapter or stub shaft. (See Section 3-5.)
- **8-2.3.2** Vertical Shaft Turbine-Type Pumps. Engines shall be connected to vertical shaft pumps by means of a right-angle gear drive with a listed flexible connecting shaft that will prevent undue strain on either the engine or gear drive. (See Section 4-5.)

Exception: Diesel engines and steam turbines designed and listed for vertical installation with vertical shaft turbine-type pumps shall be permitted to employ solid shafts and do not require a right-angle drive but do require a nonreverse ratchet.

### 8-2.4 Instrumentation and Control.

- **8-2.4.1 Governor.** Engines shall be provided with a governor capable of regulating engine speed within a range of 10 percent between shutoff and maximum load condition of the pump. The governor shall be field adjustable, set and secured to maintain rated pump speed at maximum pump load.
- **8-2.4.2** Overspeed Shutdown Device. Engines shall be provided with an overspeed shutdown device. It shall be arranged to shut down the engine at a speed approximately 20 percent above rated engine speed, and for manual reset. A means shall be provided to indicate an overspeed trouble signal to the automatic engine controller such that the controller cannot be reset until the overspeed shutdown device is manually reset to normal operating position.
- **8-2.4.3** Tachometer. A tachometer shall be provided to indicate revolutions per minute of the engine. The tachometer shall be the totalizing type, or an hour meter shall be provided to record total time of engine operation.
- **8-2.4.4** Oil Pressure Gauge. Engines shall be provided with an oil pressure gauge to indicate lubricating oil pressure.
- **8-2.4.5 Temperature Gauge.** Engines shall be provided with a temperature gauge to indicate engine coolant temperature at all times.
- **8-2.4.6 Instrument Panel.** All engine instruments shall be placed on a suitable panel secured to the engine at a suitable point.

- 8-2.4.7\* Automatic Controller Wiring in Factory. All connecting wires for automatic controllers shall be harnessed or flexibly enclosed, mounted on the engine, and connected in an engine junction box to terminals numbered to correspond with numbered terminals in the controller.
- 8-2.4.8\* Automatic Control Wiring in the Field. Interconnections between the automatic controller and engine junction box shall be made using stranded wire sized on a continuous-duty basis.
- **8-2.4.9\*** Main Battery Contactors. The main battery contactors supplying current to the starting motor shall be capable of manual mechanical operation to energize the starting motor in the event of control circuit failure.
- 8-2.4.10 Signal for Engine Running and Crank Termination. Engines shall be provided with a speed-sensitive switch to signal engine running and crank termination. Power for this signal shall be taken from a source other than the engine generator or alternator.
- **8-2.4.11 Wiring Elements.** All wiring on the engine including starting circuitry shall be sized on a continuous-duty basis.

Exception: Battery cables shall be provided per the engine manufacturer's recommendations.

- 8-2.5 Starting Methods.
- **8-2.5.1 Starting Devices.** Engines shall be equipped with a reliable starting device.
- **8-2.5.2 Electric Starting.** Where electric starting is used, the electric-starting device shall take current from a storage battery(ies).
- 8-2.5.2.1 Number and Capacity of Batteries. Each engine shall be provided with two storage battery units.
- At 40°F (4.5°C), each battery unit shall have twice the capacity sufficient to maintain the cranking speed recommended by the engine manufacturer through a 3-minute "attempt to start" cycle (15 seconds of cranking and 15 seconds of rest, in six consecutive cycles).
- **8-2.5.2.2 Battery.** Lead-acid batteries shall be furnished in a dry charge condition, with electrolyte liquid in a separate container. Electrolyte shall be added at the time the engine is put in service and the battery given a conditioning charge. Nickel-cadmium batteries shall be furnished according to the manufacturer's requirements.
- Exception: Other kinds of batteries shall be permitted to be installed in accordance with the manufacturer's requirements.
- 8-2.5.2.3\* Battery Recharging. Two means for recharging storage batteries shall be provided. One shall be the generator or alternator furnished with the engine. The other shall be an automatically controlled charger taking power from an alternating current power source.

Exception: If an alternating current power source is not available, or is not reliable, another charging method (in addition to the generator or alternator furnished with the engine) shall be provided.

### 8-2.5.2.4 Battery Chargers.

- (a) Chargers shall be specifically listed for fire pump service.
- (b) The rectifier shall be a semiconductor type.

- (c) The charger for a lead-acid battery shall be a type that automatically reduces the charging rate to less than 500 milliamperes when the battery reaches a full charge condition.
- (d) The battery charger at its rated voltage shall be capable of delivering energy into a fully discharged battery in such a manner that it will not damage the battery. It shall restore to the battery 100 percent of the battery's amperehour rating within 24 hours.
- (e) The charger shall be marked with the ampere-hour rating of the largest capacity battery that it can recharge in compliance with 8-2.5.2.4(d).
- (f) An ammeter with an accuracy of 5 percent of the normal charging rate shall be furnished to indicate the operation of the charger.
- (g) The charger shall be designed so that it will not be damaged or blow fuses during the cranking cycle of the engine when operated by an automatic or manual controller.
- (h) The charger shall automatically charge at the maximum rate whenever required by the state of charge of the battery.
- (i) Where not connected through a control panel, the battery charger shall be arranged to indicate loss of current output on the load side of the dc overcurrent protective device. [See 9-4.1.3(f).]
- | 8-2.5.2.5\* Battery Location. Storage batteries shall be rack-supported above the floor, secured against displacement, and located where they will not be subject to excessive temperature, vibration, mechanical injury, or flooding with water. They shall be readily accessible for servicing. Battery cables shall be sized in accordance with the engine manufacturer's recommendations considering the cable length required for the specific battery location.
- 8-2.5.2.6 Current-carrying parts shall not be less than 12 in. (305 mm) above the floor level.

### 8-2.5.3 Hydraulic Starting.

- 18-2.5.3.1 Where hydraulic starting is used, the accumulators and other accessories shall be cabinetized or so guarded that they are not subject to mechanical injury. The cabinet shall be installed as close to the engine as practical so as to prevent serious pressure drop between engine and cabinet. The diesel engine as installed shall be without starting aid except that a thermostatically controlled electric water jacket heater shall be employed. The diesel as installed shall be capable of carrying its full rated load within 20 seconds after cranking is initiated with the intake air, room ambient, and all starting equipment at a temperature of 32°F (0°C).
- **| 8-2.5.3.2** Hydraulic starting means shall comply with the following conditions:
- (a) The hydraulic cranking device shall be a selfcontained system that will provide the required cranking forces and engine starting RPM as recommended by the engine manufacturer.
- (b) Electrically operated means shall automatically provide and maintain the stored hydraulic pressure within the predetermined pressure limits.
- (c) The means of automatically maintaining the hydraulic system within the predetermined pressure limits shall be energized from the main bus and final emergency bus if one is provided.

- (d) Means shall be provided to manually recharge the hydraulic system.
- (e) The capacity of the hydraulic cranking system shall provide not less than six cranking cycles. Each cranking cycle (first three to be automatic from signaling source) shall provide the necessary number of revolutions at the required RPM to permit the diesel engine to meet the requirements of carrying its full rated load within 20 seconds after cranking is initiated with intake air, room ambient temperature, and hydraulic cranking system at 32°F (0°C).
- (f) Capacity of the hydraulic cranking system sufficient for three starts under conditions described in 8-2.5.3.2(e) shall be held in reserve and arranged so that the operation of a single control by one person will permit the reserve capacity to be employed.
- (g) All controls for engine shutdown in event of low engine lube, overspeed, and high water jacket temperature shall be 12- or 24-volt dc source to accommodate controls supplied on engine. In the event of such failure, the hydraulic cranking system will provide an interlock to prevent the engine from recranking. The interlock shall be manually reset for automatic starting when engine failure is corrected.

### 8-2.5.4 Air Starting.

- **8-2.5.4.1 Existing Requirements.** In addition to the requirements in Section 8-1 through 8-2.4.6, 8-2.5.1, 8-2.6 through 8-6.2, 8-6.4, and 8-6.5, the following sections shall apply.
- | 8-2.5.4.2 Automatic Controller Connections in Factory. All conductors for automatic controllers shall be harnessed or flexibly enclosed, mounted on the engine, and connected in an engine junction box to terminals numbered to correspond with numbered terminals in the controller. This is to ensure ready connection in the field between the two sets of terminals.
- 8-2.5.4.3 Signal for Engine Running and Crank Termination. Engines shall be provided with a speed-sensitive switch to signal running and crank termination. Power for this signal shall be taken from a source other than the engine compressor.

### 8-2.5.4.4\* Air Starting Supply.

- **8-2.5.4.4.1** The air supply container shall be sized for 180 seconds of continuous cranking without recharging. There shall be a separate, suitably powered automatic air compressor or means of obtaining air from some other system, independent of the compressor driven by the fire pump engine. Suitable supervisory service shall be maintained to indicate high and low air pressure conditions.
- | 8-2.5.4.4.2 A bypass conductor with a manual valve or switch shall be installed for direct application of air from the air container to the engine starter in the event of control circuit failure.

### 8-2.6 Engine Cooling.

- 8-2.6.1 The engine cooling system shall be included as part of the engine assembly and shall be one of the following closed-circuit types:
- (a) A heat exchanger type that includes a circulating pump driven by the engine, a heat exchanger, and an engine jacket temperature regulating device; or
- (b) A radiator type that includes a circulating pump driven by the engine, a radiator, an engine jacket temperature regulating device, and an engine-driven fan for providing positive movement of air through the radiator.

**8-2.6.2 Coolant and Fill Openings.** An opening shall be provided in the circuit for filling the system, checking coolant level, and adding make-up coolant when required. The coolant shall comply with the recommendation of the engine manufacturer.

### 8-2.6.3\* Heat Exchanger Water Supply.

(a) Supply. The cooling water supply for a heat exchanger type system shall be from the discharge of the pump, taken off prior to the pump discharge valve. Threaded rigid piping shall be used for this connection. The pipe connection in the direction of flow shall include an indicating manual shutoff valve, an approved flushing-type strainer in addition to the one that can be a part of the pressure regulator, a pressure regulator, an automatic valve listed for fire protection service, and a second indicating manual shutoff valve. A pressure gauge shall be installed in the cooling water supply system on the engine side of the last manual valve.

Exception: The automatic valve is not required on a vertical shaft turbine-type pump or any other pump when there is no pressure in the discharge when the pump is idle.

- (b) Pressure Regulator. The pressure regulator shall be of such size and type that it is capable of and adjusted for passing approximately 120 percent of the cooling water required when the engine is operating at maximum brake horse-power and when the regulator is supplied with water at the pressure of the pump when it is pumping at 150 percent of its rated capacity. The cooling water flow required shall be set based on the maximum ambient cooling water.
- (c) Automatic Valve. An automatic valve permit flow of cooling water to the engine when it is running.
- 8-2.6.4\* Heat Exchanger Water Supply Bypass. A bypass line with manual valves, a flush-type strainer, and a pressure regulator shall be installed around the manual shutoff valve, strainer, pressure regulator, and automatic valve.

### 8-2.6.5 Heat Exchanger Waste Outlet.

**8-2.6.5.1** An outlet shall be provided for the wastewater line from the heat exchanger, and the discharge line shall not be less than one size larger than the inlet line. The outlet line shall be as short as practical, shall provide discharge into a visible open waste cone, and shall have no valves in it.

Exception: It shall be permitted to discharge to a suction reservoir provided a visual flow indicator and temperature indicator are installed.

8-2.6.5.2 When the waste outlet piping is longer than 15 ft (4.8 m) and/or its outlet discharges more than 4 ft (1.2 m) higher than the heat exchanger, the pipe size shall be increased by at least one size.

### 8-2.6.6 Radiators.

8-2.6.6.1 The heat from the primary circuit of a radiator shall be dissipated by a fan included with, and driven by, the engine. The radiator shall be designed to limit maximum engine operating temperature with an inlet air temperature of 120°F (49°C) at the combustion air cleaner inlet. The radiator shall include the plumbing to the engine and a flange on the air discharge side for the connection of a flexible duct to the discharge air ventilator.

8-2.6.6.2 The fan shall push the air through the radiator to be exhausted from the room via the air discharge ventilator. To ensure adequate air flow through the room and radiator, the radiator cooling package shall be capable of a 0.5 in. (13 mm) water column restriction created by the combination of the air supply and the discharge ventilators. This external restriction shall be in addition to the radiator, fan guard, and other engine component obstructions. The fan shall be guarded for personnel protection.

### 8-3\* Pump and Engine Protection.

8-3.1 Pump Room Drainage. The floor or surface around the pump and engine shall be pitched for adequate drainage of escaping water away from critical equipment, such as pump, engine, controller, fuel tank, etc.

### 8-3.2\* Ventilation. Ventilation shall be provided to:

- (a) Control the maximum temperature to 120°F (49°C) at the combustion air cleaner inlet with engine running at rated load;
  - (b) Supply air for engine combustion;
  - (c) Remove any hazardous vapors;
- (d) Supply and exhaust air as necessary for radiator cooling of the engine, when required.

The ventilation system components shall be coordinated with the engine operation.

- 8-3.2.1\* Air Supply Ventilator. The air supply ventilator shall be considered to include anything in the air supply path to the room. The total air supply path to the pump room shall not restrict the flow of the air more than 0.2 in. (5.1 mm) water column.
- 8-3.2.2\* Air Discharge Ventilator. The air discharge ventilator shall be considered to include anything in the air discharge path from the room. The air discharge ventilator shall allow sufficient air to exit the pump room to satisfy 8-3.2.

For radiator-cooled engines, the radiator discharge shall be ducted outdoors in a manner that will prevent recirculation. The duct shall be attached to the radiator via a flexible section. The air discharge path, for radiator-cooled engines, shall not restrict the flow of air more than 0.3 in. (7.6 mm) water column.

Exception: A recirculation duct is acceptable for cold weather operation providing that:

- (a) The recirculation air flow is regulated by a thermostatically controlled damper.
  - (b) The control damper fully closes in a failure mode.
- (c) The recirculated air is ducted to prevent direct recirculation to the radiator.
- (d) It will not cause the temperature at the combustion air cleaner inlet to rise above 120°F (49°C).

### 8-4 Fuel Supply and Arrangement.

- **8-4.1 Plan Review.** Before any fuel system is installed, plans shall be prepared and submitted to the authority having jurisdiction for agreement on suitability of the system for conditions prevailing.
- **8-4.2 Guards.** A guard or protecting pipe shall be provided for all exposed fuel lines.

- 8-4.3\* Fuel Tank Capacity. Fuel supply tank(s) shall have a capacity at least equal to 1 gal per horsepower (5.07 L/kW), plus 5 percent volume for expansion and 5 percent volume for sump. Larger capacity tanks might be required and shall be determined by prevailing conditions, such as refill cycle and fuel heating due to recirculation, and shall be subject to special conditions in each case. The fuel supply tank and fuel shall be reserved exclusively for the fire pump diesel engine.
- **8-4.4** Multiple Pumps. There shall be a separate fuel line and separate fuel supply tank for each engine.
- 8-4.5\* Fuel Supply Location. Diesel fuel supply tanks shall be located aboveground in accordance with municipal or other ordinances and in accordance with requirements of the authority having jurisdiction, and shall not be buried. The engine fuel supply (suction) connection shall be located on the tank so that 5 percent of the tank volume provides a sump volume not usable by the engine. The fuel supply shall be located on a side of the tank at the level of the 5 percent sump volume. The inlet to the fuel supply line shall be located so that its opening is no lower than the level of the engine fuel transfer pump. The engine manufacturer's fuel pump static head pressure limits shall not be exceeded when the level of fuel in the tank is at a maximum. The fuel return line shall be installed per the engine manufacturer's recommendation. In zones where freezing [32°F (0°C)] might be encountered, the fuel tanks shall be located in the pump room. Means other than sight tubes shall be provided for determining the amount of fuel in each storage tank. Each tank shall have suitable fill, drain, and vent connections.
- 8-4.6\* Fuel Piping. Flame-resistant flexible hoses listed for this service shall be provided at the engine for connection to fuel system piping. There shall be no shutoff valve in the fuel return line to the tank.
- 8-4.7\* The type and grade of diesel fuel shall be as specified by the engine manufacturer. Residual fuels, domestic heating furnace oils, and drained lubrication oils shall not be used.
- **8-4.8 Fuel Solenoid Valve.** Where an electric solenoid valve is used to control the engine fuel supply, it shall be capable of manual mechanical operation or of being manually bypassed in the event of a control circuit failure.

### 8-5 Engine Exhaust.

- **8-5.1 Independent Exhaust.** Each pump engine shall have an independent exhaust system.
- 8-5.2 Exhaust Discharge Location. Exhaust from the engine shall be piped to a safe point outside the pump room and arranged to exclude water. Exhaust gases shall not be discharged where they will affect persons or endanger buildings.
- 8-5.3\* Exhaust Piping. A seamless or welded corrugated (not interlocked) flexible connection shall be made between the engine exhaust outlet and exhaust pipe. The exhaust pipe shall not be any smaller than the engine exhaust outlet and shall be as short as possible. The exhaust pipe shall be covered with high-temperature insulation or otherwise guarded to protect personnel from injury. The exhaust pipe and muffler, if used, shall be suitable for the use intended, and the exhaust back pressure shall not exceed the engine manufacturer's recommendations.

Exhaust pipes shall terminate outside the structure at a point where the hot gases or sparks will discharge harmlessly and not be directed against combustible materials or structures, or into atmospheres containing flammable gases or vapors or combustible dusts. Exhaust pipes shall not terminate under loading platforms or structures, or near ventilation air inlets.

Exhaust pipes shall be installed with clearances of at least 9 in. (229 mm) to combustible materials.

Exception No. 1: Exhaust pipes passing directly through combustible roofs shall be guarded at the point of passage by ventilated metal thimbles that extend not less than 9 in. (229 mm) above and 9 in. (229 mm) below roof construction and are at least 6 in. (152 mm) in diameter larger than the exhaust pipe.

Exception No. 2: Exhaust pipes passing directly through combustible walls or partitions shall be guarded at the point of passage by one of the following methods:

- (a) Metal ventilated thimbles not less than 12 in. (305 mm) larger in diameter than the exhaust pipe; or
- (b) Metal or burned clay thimbles built in brickwork or other approved materials providing not less than 8 in. (203 mm) of insulation between the thimble and construction material.
- 8-5.4 Exhaust Manifold. Exhaust manifolds shall incorporate provisions to avoid hazard to the operator or to flammable material adjacent to the engine.

### 8-6\* Driver System Operation.

- 8-6.1 Weekly Run. Engines shall be started no less than once a week and run for no less than 30 minutes to attain normal running temperature. They shall run smoothly at rated speed.
- 8-6.2 System Performance. Engines shall be kept clean, dry, and well lubricated to ensure adequate performance. [See NFPA 25, Standard for the Inspection, Testing, and Maintenance of Water-Based Fire Protection Systems, for proper maintenance of engine(s), batteries, fuel supply, and environmental conditions.]

### 8-6.3 Battery Maintenance.

- **8-6.3.1** Storage batteries shall be kept charged at all times. They shall be tested frequently to determine the condition of the battery cells and the amount of charge in the battery.
- **8-6.3.2** Only distilled water shall be used in battery cells. The plates shall be kept submerged at all times.
- 8-6.3.3 The automatic feature of a battery charger is not a substitute for proper maintenance of battery and charger. Periodic inspection of both shall be made. This inspection shall determine that the charger is operating correctly, the water level in the battery is correct, and the battery is holding its proper charge.
- 8-6.4 Fuel Supply Maintenance. The fuel storage tanks shall be kept as full as possible at all times, but never less than 50 percent of tank capacity. They shall always be filled by means that will ensure removal of all water and foreign material.
- 8-6.5\* Temperature Maintenance. Temperature of the pump room, pump house, or area where engines are installed shall never be less than the minimum recommended by the engine manufacturer. An engine jacket water heater shall be provided to maintain 120°F (49°C).

- The engine manufacturer's recommendations for oil heaters shall be followed.
- 8-6.6 Emergency Starting and Stopping. The sequence for emergency manual operation, arranged in a step-by-step manner, shall be posted on the fire pump engine. It shall be the engine manufacturer's responsibility to list any specific instructions pertaining to the operation of this equipment during the above-mentioned sequences.

### **Chapter 9 Engine Drive Controllers**

9-1 Application. This chapter provides requirements for minimum performance of automatic/nonautomatic diesel engine controllers for diesel-engine-driven fire pumps. Accessory devices, such as alarm monitoring and signaling means, are included when necessary to ensure minimum performance of the aforementioned equipment.

### 9-1.1 General.

- **9-1.1.1** All controllers shall be specifically listed for dieselengine-driven fire pump service.
- 9-1.1.2 All controllers shall be completely assembled, wired, and tested by the manufacturer before shipment from the factory.
- 9-1.1.3 All controllers shall be marked "Diesel Engine Fire Pump Controller" and shall show plainly the name of the manufacturer, the identifying designation, and the complete electrical rating. Where multiple pumps are provided, one or more serving different areas or portions of the facility, an appropriate sign shall be conspicuously attached to each controller indicating the area, zone, or portion of the system served by that pump or pump controller.
- 9-1.1.4 It shall be the responsibility of the pump manufacturer or its designated representative to make necessary arrangements for the services of a controller manufacturer's representative, when needed, for services and adjustment of the equipment during the installation, testing, and warranty periods.

### 9-2 Location.

- 9-2.1\* Controllers shall be located as close as is practical to the engines they control and shall be within sight of the engines.
- 9-2.2 Controllers shall be so located or so protected that they will not be injured by water escaping from pumps or pump connections. Current-carrying parts of controllers shall not be less than 12 in. (305 mm) above the floor level.
- **9-2.3** Working clearances around controllers shall comply with NFPA 70, *National Electrical Code*, Article 110.

### 9-3 Construction.

- 9-3.1\* Equipment. All equipment shall be suitable for use in locations subject to a moderate degree of moisture, such as a damp basement. Reliability of operation shall not be adversely affected by normal dust accumulations.
- **9-3.2 Mounting.** All equipment not mounted on the engine shall be mounted in a substantial manner on a single noncombustible supporting structure.

<sup>&</sup>lt;sup>1</sup>Indicates extracted text from NFPA 37, Standard for the Installation and Use of Stationary Combustion Engines and Gas Turbines.

### 9-3.3 Enclosures.

- 9-3.3.1 The structure or panel shall be securely mounted in a NEMA Type 2 dripproof, as a minimum, enclosure(s) (see NEMA Standard 250). Where the equipment is located outside or special environments exist, suitably rated enclosures shall be used.
- 9-3.3.2 Grounding. The enclosures shall be grounded in accordance with NFPA 70, National Electrical Code, Article 250.
- 9-3.4 Locked Cabinet. All switches required to keep the controller in the "automatic" position shall be within locked cabinets having break glass panels.

### 9-3.5 Connections and Wiring.

- 9-3.5.1 Field Wiring. All wiring between the controller and the diesel engine shall be stranded and sized to carry the charging or control currents as required by the controller manufacturer. Such wiring shall be protected against mechanical injury. Controller manufacturer's specifications for distance and wire size shall be followed.
- **9-3.5.2** Wiring Elements. Wiring elements of the controller shall be designed on a continuous-duty basis.
- 9-3.5.3 A diesel engine fire pump controller shall not be used as a junction box to supply other equipment. Electrical supply conductors for pressure maintenance (jockey or make-up) pump(s) shall not be connected to the diesel engine fire pump controller.

### 9-3.6 Electrical Diagrams and Instructions.

- **9-3.6.1** A field connection diagram shall be provided and permanently attached to the inside of the enclosure.
- **9-3.6.2** The field connection terminals shall be plainly marked to correspond with the field connection diagram furnished.
- 9-3.6.3 For external engine connections, the field connection terminals shall be commonly numbered between the controller and engine terminals.
- 9-3.7 Marking. Each operating component of the controller shall be marked to plainly indicate an identification symbol appearing on the electrical schematic diagram. The markings shall be located so as to be visible after installation.
- 9-3.8\* Instructions. Complete instructions covering the operation of the controller shall be provided and conspicuously mounted on the controller.

### 9-4 Components.

- 9-4.1 Alarm and Signal Devices on Controller.
- **9-4.1.1 Visible Indicators.** All visible indicator alarms shall be plainly visible.
- **9-4.1.2\*** Visible indication shall be provided to indicate that the controller is in the "automatic" position. If the visible indicator is a pilot lamp, it shall be accessible for replacement.
- 9-4.1.3 Separate visible indicators and a common audible alarm capable of being heard while the engine is running and operable in all positions of the main switch except "off" shall be provided to indicate trouble caused by the following conditions:

- (a) Critically low oil pressure in the lubrication system. The controller shall provide means for testing the position of the pressure switch contacts without causing trouble alarms.
  - (b) High engine jacket coolant temperature.
  - (c) Failure of engine to start automatically.
  - (d) Shutdown from overspeed.
- (e) Battery failure. Each controller shall be provided with a separate visible indicator for each battery.
- (f) Battery charger failure. Each controller shall be provided with a separate visible indicator for battery charger failure.

Exception: The audible alarm shall not be required for battery charger failure.

- (g) Low air or hydraulic pressure. Where air or hydraulic starting is provided (see 8-2.5 and 8-2.5.4), each pressure tank shall provide to the controller separate visible indicators to alarm low pressure.
- **9-4.1.4** No audible alarm silencing switch, other than the controller main switch, shall be permitted for the alarms required in 9-4.1.3.
- 9-4.1.5 Where audible alarms for the conditions listed in A-2-18 are incorporated with the engine alarms specified in 9-4.1.3, a silencing switch for the A-2-18 audible alarms shall be provided at the controller. The circuit shall be so arranged that the audible alarm will be activated if the silencing switch is in the "silent" position when the supervised conditions are normal.
- 9-4.2 Alarm and Signal Devices Remote from Controller. Where the pump room is not constantly attended, audible or visible alarms powered by a source other than the engine starting batteries and not exceeding 125 volts shall be provided at a point of constant attendance. These alarms shall indicate the following:
  - (a) Engine running (separate signal),
- (b) The controller main switch has been turned to "off" or "manual" position (separate signal), and
- (c)\* Trouble on the controller or engine (separate or common signals). (See 9-4.1.3.)
- 9-4.3 Controller Alarm Contacts for Remote Indication. Controllers shall be equipped with contacts (open or closed) to operate circuits for the conditions covered in 9-4.2.
- 9-4.4 Pressure Recorder. The controller shall be equipped with a pressure-recording device that shall operate continuously for at least 7 days without resetting or rewinding. The pressure-recording device shall be spring wound mechanically or driven by reliable electrical means. The pressure-recording device shall not be solely dependent upon ac electric power as its primary power source. Upon loss of ac electric power, the electric-driven recorder shall be capable of at least 24 hours of operation.

Exception: In a nonpressure-actuated controller, the pressure recorder shall not be required.

### 9-5\* Starting and Control.

### 9-5.1 Automatic and Nonautomatic.

9-5.1.1 An automatic controller shall be operable also as a nonautomatic controller.

**9-5.1.2** The controller's primary source of power shall not be ac electric power.

### 9-5.2 Automatic Operation of Controller.

- 9-5.2.1 Water Pressure Control. The controller circuit shall be provided with a pressure-actuated switch having independent high- and low-calibrated adjustments. There shall be no pressure snubber or restrictive orifice employed within the pressure switch. This switch shall be responsive to water pressure in the fire protection system. The pressure-sensing element of the switch shall be capable of a momentary surge pressure of 400 psi (27.6 bars) minimum without losing its accuracy. Suitable provision shall be made for relieving pressure to the pressure-actuated switch to allow testing of the operation of the controller and the pumping unit. [See Figures A-7-5.2.1(a) and (b).]
- (a) For all pump installations (including jockey pumps), each controller shall have its own individual pressure sensing line.
- (b) The pressure-sensing line connection for each pump (including jockey pumps) shall be made between that pump's discharge check valve and discharge control valve. This line shall be corrosion-resistant metallic pipe or tube and fittings (brass, copper, or series 300 stainless steel) of  $\frac{1}{2}$ -in. nominal size. There shall be two check valves installed in the pressure sensing line at least 5 ft (1.6 m) apart with a  $\frac{3}{32}$ -in. (2.4-mm) hole drilled in the clapper to serve as a damper. [See Figures A-7-5.2.1(a) and (b) for clarification.]
- Exception No. 1: If water is clean, ground-face unions with non-corrosive diaphragms drilled with 3/32-in. (2.4-mm) orifices shall be permitted in place of the check valves.
- Exception No. 2: In a nonpressure-actuated controller, the pressure-actuated switch shall not be required.
- 9-5.2.2 Fire Protection Equipment Control. Where the pump supplies special water control equipment (deluge valves, dry-pipe valves, etc.), it might be desirable to start the engine before the pressure-actuated switch(es) would do so. Under such conditions the controller shall be equipped to start the engine upon operation of the fire protection equipment.
- 9-5.2.3 Manual Electric Control at Remote Station. Additional control stations for causing nonautomatic, continuous operation of the pumping unit, independent of the pressure-actuated control switch, shall be permitted to be provided at locations remote from the controller. Such stations shall not be operable to stop the unit except through the established operation of the running period timer circuit when the controller is arranged for automatic shutdown. [See 9-5.4.2(a).]
- | 9-5.2.4 Sequence Starting of Pumps. The controller for each unit of multiple pump units shall incorporate a sequential timing device to prevent any one engine from starting simultaneously with any other engine. Each pump supplying suction pressure to another pump shall be arranged to start before the pump it supplies. If water requirements call for more than one pumping unit to operate, the units shall start at intervals of 5 to 10 seconds. Failure of a leading engine to start shall not prevent subsequent engines from starting.
- 9-5.2.5 External Circuits Connected to Controllers. With pumping units operating singly or in parallel, the control circuits entering or leaving the fire pump controller shall be so arranged as to prevent failure to start due to fault. Breakage,

disconnecting, shorting of the wires, or loss of power to these circuits might cause continuous running of the fire pump but shall not prevent the controller(s) from starting the fire pump(s) due to causes other than these external circuits.

**9-5.2.6 Sole Supply Pumps.** Shutdown shall be accomplished by manual or automatic means.

Exception: Automatic shutdown shall not be permitted where the pump constitutes the sole source of supply of a fire sprinkler or standpipe system or where the authority having jurisdiction has required manual shutdown.

9-5.2.7 Weekly Program Timer. To ensure dependable operation of the engine and its controller, the controller equipment shall be arranged to automatically start and run the engine for at least 30 minutes once a week. Means shall be permitted within the controller to manually terminate the weekly test provided a minimum of 30 minutes has expired. A solenoid valve drain on the pressure control line shall be the initiating means.

Performance of this weekly program timer shall be recorded as a pressure drop indication on the pressure recorder. (See 9-4.4.)

Exception: In a nonpressure-actuated controller, the weekly test shall be permitted to be initiated by means other than a solenoid valve.

### 9-5.3 Nonautomatic Operation of Controller.

**9-5.3.1** Manual Control at Controller. There shall be a manually operated switch on the controller panel. This switch shall be so arranged that operation of the engine, when manually started, cannot be affected by the pressure-actuated switch. The arrangement shall also provide that the unit will remain in operation until manually shut down.

The controller shall be arranged to manually start the engine by opening the solenoid valve drain when so initiated by the operator.

### 9-5.3.2 Starting Equipment Arrangement.

- (a) Two storage battery units, each complying with the requirements of 8-2.5.2, shall be provided and so arranged that manual and automatic starting of the engine can be accomplished with either battery unit. The starting current shall be furnished by first one battery and then the other on successive operations of the starter. The changeover shall be made automatically, except for manual start.
- (b) In the event that the engine does not start after completion of its "attempt to start" cycle, the controller shall stop all further cranking and operate a visible indicator and audible alarm on the controller. The "attempt to start" cycle shall be fixed and shall consist of 6 crank periods of an approximately 15-second duration separated by 5 rest periods of an approximately 15-second duration.
- (c) In the event that one battery is inoperative or missing, the control shall lock-in on the remaining battery unit during the cranking sequence.

### 9-5.4 Methods of Stopping.

- **9-5.4.1 Manual Electric Shutdown.** Manual shutdown shall be accomplished by either of the following:
  - (a) Operation of the main switch inside the controller, or
- (b) Operation of a stop button on the outside of the controller enclosure. This shall cause engine shutdown through

the automatic circuits only if all starting causes have been returned to normal. The controller shall then return to the full automatic position.

### 9-5.4.2\* Automatic Shutdown After Automatic Start.

- (a) If the controller is set up for automatic engine shutdown, the controller shall shut down the engine only after all starting causes have returned to normal and a 30-minute minimum run time has elapsed.
- (b) When the engine emergency overspeed device operates, the controller shall remove power from the engine running devices, prevent further cranking, energize the overspeed alarm, and lock-out until manually reset. Resetting of the overspeed circuit shall be required at the engine and by resetting the controller main switch to the "off" position.
- (c) The engine shall not shut down automatically on high water temperature or low oil pressure when any starting cause exists. If no other starting cause exists during engine test, shutdown shall be permitted.
- (d) The controller shall not be capable of being reset until the engine overspeed shutdown device is manually reset.
- 9-5.5 Emergency Control. Automatic control circuits, the failure of which could prevent engine starting and running, shall be completely bypassed during manual start and run.

### 9-6 Air Starting Engine Controllers.

- 9-6.1 Existing Requirements. In addition to the requirements in Section 9-1 and 9-1.1.1, 9-1.1.4 through 9-3.4, 9-3.8, 9-5 through 9-5.2.1(b), 9-5.2.4, 9-5.2.7, and 9-5.4.2 through 9-5.5, the following sections shall apply.
- **9-6.2** All controllers shall be completely assembled and tested by the manufacturer before shipment from the factory.
- 9-6.3 All controllers shall be marked "Diesel Engine Fire Pump Controller" and shall show plainly the name of the manufacturer, the identifying designation, and the complete rating. Where multiple pumps are provided, one or more serving different areas or portions of the facility, an appropriate sign shall be conspicuously attached to each controller indicating the area, zone, or portion of the system served by that pump or pump controller.

### 9-6.4 Connections.

- **9-6.4.1 Field Connections.** All conductors from the panel to the engine and starter support shall have adequate current-carrying capacity. Such conductors shall be protected against mechanical injury. Controller manufacturer's specifications for distance and conductor size shall be followed.
- 9-6.4.2 Conductor Elements. Conductor elements of the controller shall be designed to operate on a continuous-duty basis.
- 9-6.5 Circuit Diagrams and Instructions. A circuit diagram shall be provided and permanently attached to the inside of the enclosure showing exact circuitry for the controller, including identifying numbers of individual components. All circuit terminals shall be plainly and commonly marked and numbered to correspond with the circuit diagram furnished. For external engine connections, the connection strips shall be commonly numbered.
- 9-6.6 Marking. Each operating component of the controller shall be marked to plainly indicate an identifying number

referenced to the circuit diagram. The markings shall be located so as to be visible after installation.

### 9-6.7 Alarm and Signal Devices on Controller.

- **9-6.7.1** A visual indicator(s) shall be provided to indicate that the controller is in the "automatic" position. The visual indicator shall be accessible for replacement.
- **9-6.7.2** Separate visual indicators and a common audible alarm shall be provided to indicate trouble caused by the following conditions:
- (a) Critically low oil pressure in the lubrication system. The controller shall provide means for testing the position of the pressure switch contacts without causing trouble alarms.
  - (b) High engine jacket coolant temperature.
  - (c) Failure of engine to start automatically.
  - (d) Shutdown from overspeed.
- (e) Low air pressure. The air supply container shall be provided with a separate visible indicator to indicate low air pressure.
- 9-6.7.3 No audible alarm silencing switch or valve, other than the controller main switch or valve, shall be permitted for the alarms in 9-6.7.2.
- 9-6.7.4 Where audible alarms for the conditions listed in A-2-18 are incorporated with the engine alarms specified in 9-6.7.2, a silencing switch or valve for the A-2-18 audible alarms shall be provided at the controller. The circuit shall be so arranged that the audible alarm will be activated if the silencing switch or valve is in the "silent" position when the supervised conditions are normal.
- 9-6.8 Alarms for Remote Indication. Controllers shall be equipped to operate circuits for remote indication of the conditions covered in 9-4.1.3 and 9-4.2(a) through (c).
- 9-6.9 Pressure Recorder. The controller shall be equipped with a pressure-recording device that shall operate continuously for at least 7 days without resetting or rewinding. The pressure-recording device shall be spring wound mechanically, air powered, or driven by reliable electrical means. The pressure-recording device shall not be solely dependent upon ac electric power as its primary power source. Upon loss of ac electric power, the electric-driven recorder shall be capable of at least 24 hours of operation.

Exception: In a nonpressure-actuated controller, the pressure recorder shall not be required.

- 9-6.10 Fire Protection Equipment Control. Where the pump supplies special water control equipment (deluge valves, dry-pipe valves, etc.), it might be desirable to start the engine before the pressure-actuated valve or switch would do so. Under such conditions the controller shall be equipped to start the engine upon operation of the fire protection equipment.
- 9-6.11 Manual Control at Remote Station. Additional control stations for causing nonautomatic, continuous operation of the pumping unit, independent of the pressure-actuated control valve or switch, might be provided at locations remote from the controller. Such stations shall not be operable to stop the unit except through the established operation of the running period timer circuit when the controller is arranged for automatic shutdown. (See 9-5.4.2.)

- 9-6.12 External Circuits Connected to Controllers. With pumping units operating singly or in parallel, the control conductors entering or leaving the fire pump controller shall be so arranged as to prevent failure to start due to fault. Breakage, disconnecting, or loss of power to these conductors might cause continuous running of the fire pump, but shall not prevent the controller(s) from starting the fire pump(s).
- 9-6.13 Sole Supply Pumps. For sprinkler or standpipe systems where an automatically controlled pumping unit constitutes the sole supply, the controller shall be arranged for manual shutdown. Manual shutdown shall also be provided where required by the authority having jurisdiction.
- 9-6.14 Manual Control at Controller. There shall be a manually operated valve or switch on the controller panel. This valve or switch shall be so arranged that operation of the engine, when manually started, cannot be affected by the pressure-actuated switch. The arrangement shall also provide that the unit will remain in operation until manually shut down.

### 9-6.15 Starting Equipment Arrangement.

- (a) The air supply container, complying with the requirements of 8-2.5.4.4, shall be provided and so arranged that manual and automatic starting of the engine can be accomplished.
- (b) In the event that the engine does not start after completion of its "attempt to start" cycle, the controller shall stop all further cranking and operate the audible and visible alarms. The "attempt to start" cycle shall be fixed and shall consist of one crank period of an approximately 90-second duration.
- 9-6.16 Manual Shutdown. Manual shutdown shall be accomplished by either of the following:
- (a) Operation of a stop valve or switch on the controller panel, or
- (b) Operation of a stop valve or switch on the outside of the controller enclosure. This shall cause engine shutdown through the automatic circuits only after starting causes have been returned to normal. This action shall return the controller to full automatic position.

### Chapter 10 Steam Turbine Drive

### 10-1 General.

### 10-1.1 Acceptability.

- 10-1.1.1 Steam turbines of adequate power are acceptable prime movers for driving fire pumps. Reliability of the turbines shall have been proved in commercial work.
- **10-1.1.2** The steam turbine shall be directly connected to the fire pump.

### 10-1.2 Turbine Capacity.

- 10-1.2.1 For steam boiler pressures not exceeding 120 psi (8 bars) gauge, the turbine shall be capable of driving the pump at its rated speed and maximum pump load with a pressure as low as 80 psi (5.5 bars) gauge at the turbine throttle, when exhausting against atmospheric back pressure, with the hand valve open.
- 10-1.2.2 For steam boiler pressures exceeding 120 psi (8 bars) gauge, where steam is continuously maintained, a

- pressure 70 percent of the usual boiler pressure shall take the place of the 80 psi (5.5 bars) pressure required in 10-1.2.1.
- 10-1.2.3 In ordering turbines for centrifugal fire pumps, the purchaser shall specify the rated and maximum pump loads at rated speed, the rated speed, the boiler pressure, the steam pressure at the turbine throttle (if possible), and the steam superheat.
- 10-1.3\* Steam Consumption. Prime consideration shall be given to the selection of a turbine having a total steam consumption commensurate with the steam supply available. Where multistage turbines are used, they shall be so designed that the pump can be brought up to speed without a warmup time requirement.

### 10-2\* Turbine.

### 10-2.1 Casing and Other Parts.

- 10-2.1.1\* The casing shall be designed to permit access with the least possible removal of parts or piping.
- 10-2.1.2 A safety valve shall be connected directly to the turbine casing to relieve high steam pressure in the casing.
- 10-2.1.3 The main throttle valve shall be located in a horizontal run of pipe connected directly to the turbine. There shall be a water leg on the supply side of the throttle valve. This leg shall be connected to a suitable steam trap to automatically drain all condensate from the line supplying steam to the turbine. Steam and exhaust chambers shall be equipped with suitable condensate drains. Where the turbine is automatically controlled, these drains shall discharge through adequate traps. In addition, if the exhaust pipe discharges vertically, there shall be an open drain at the bottom elbow. This drain shall not be valved but shall discharge to a safe location.
- 10-2.1.4 The nozzle chamber, governor-valve body, pressure regulator, and other parts through which steam passes shall be made of a metal able to withstand the maximum temperatures involved.

### 10-2.2 Speed Governor.

- 10-2.2.1 The steam turbine shall be equipped with a speed governor set to maintain rated speed at maximum pump load. The governor shall be capable of maintaining, at all loads, the rated speed within a total range of approximately 8 percent from no turbine load to full rated turbine load:
- (a) With normal steam pressure and with hand valve closed, or
- (b) With steam pressures down to 80 psi (5.5 bars) gauge [or down to 70 percent of full pressure where this is in excess of 120 psi (8 bars)] and with hand valve open.
- 10-2.2.2 While the turbine is running at rated pump load, the speed governor shall be capable of adjustment to secure speeds approximately 5 percent above and 5 percent below the rated speed of the pump.
- 10-2.2.3 There shall also be provided an independent emergency governing device. It shall be arranged to shut off the steam supply at a turbine speed approximately 20 percent higher than the rated pump speed.

### 10-2.3 Gauge and Gauge Connections.

10-2.3.1 A listed steam pressure gauge shall be provided on the entrance side of the speed governor. A 1/4-in. pipe tap for a gauge connection shall be provided on the nozzle chamber of the turbine.

10-2.3.2 The gauge shall indicate pressures not less than one and one-half times the boiler pressure, and in no case less than 240 psi (16 bars), and shall be marked "Steam."

10-2.4 Rotor. The rotor of the turbine shall be of suitable material. The first unit of a rotor design shall be type tested in the manufacturer's shop at 40 percent above rated speed. All subsequent units of the same design shall be tested at 25 percent above rated speed.

### 10-2.5 Shaft.

10-2.5.1 The shaft of the turbine shall be of high-grade steel, such as open-hearth carbon steel or nickel steel.

10-2.5.2 Where the pump and turbine are assembled as independent units, a flexible coupling shall be provided between the two units.

**10-2.5.3** Where an overhung rotor is used, the shaft for the combined unit shall be in one piece with only two bearings.

10-2.5.4 The critical speed of the shaft shall be well above the highest speed of the turbine so that the turbine will operate at all speeds up to 120 percent of rated speed without objectionable vibration.

10-2.6 Bearings. Turbines having sleeve bearings shall have split-type bearing shells and caps.

Exception: Turbines having ball bearings shall be acceptable after they have established a satisfactory record in the commercial field. Means shall be provided to give visual indication of the oil level.

10-3\* Installation. Details of steam supply, exhaust, and boiler feed need to be carefully planned to provide reliability and effective operation of a steam-turbine-driven fire pump.

# Chapter 11 Acceptance Testing, Performance, and Maintenance

### 11-1 Hydrostatic Tests and Flushing.

11-1.1 Piping (suction and discharge) shall be hydrostatically tested at not less than 200 psi (13.8 bars) pressure, or at 50 psi (3.4 bars) in excess of the maximum pressure to be maintained in the system, whichever is greater. The pressure shall be maintained for 2 hours.

11-1.2 Suction piping shall be flushed at a flow rate not less than indicated in Table 11-1.2 or at the hydraulically calculated water demand rate of the system, whichever is greater.

11-1.3 The installing contractor shall furnish a certificate of test prior to the start of the fire pump field acceptance test.

### 11-2 Field Acceptance Tests.

11-2.1 The pump manufacturer, the engine manufacturer (when supplied), the controller manufacturer, and the transfer switch manufacturer (when supplied) (or their respective representatives) shall be present for the field acceptance test. (See Section 1-6.)

Table 11-1.2 Flow Rate

Pipe	F	low
Size (In.)	GPM	L/min
4	590	2233
5	920	3482
6	1360	5148
8	2350	8895
10	3670	13,891
12	5290	20,023

11-2.1.1 All electric wiring to the fire pump motor(s), including control (multiple pumps) interwiring, emergency power supply, and jockey pump, shall be completed and checked by the electrical contractor prior to the initial startup and acceptance test.

11-2.2\* • The authority having jurisdiction shall be notified as to time and place of the field acceptance test.

11-2.3 A copy of the manufacturer's certified pump test characteristic curve shall be available for comparison of results of field acceptance test. The fire pump as installed shall equal the performance as indicated on the manufacturer's certified shop test characteristic curve within the accuracy limits of the test equipment.

11-2.4 The fire pump shall perform at minimum, rated, and peak loads without objectionable overheating of any component.

11-2.5 Vibrations of the fire pump assembly shall not be of a magnitude to warrant potential damage to any fire pump component.

### 11-2.6\* Field Acceptance Test Procedures.

11-2.6.1\* Test Equipment. Test equipment shall be provided to determine net pump pressures, rate of flow through the pump, volts and amperes for electric-motor-driven pumps, and speed.

11-2.6.2\* Flow Tests. The minimum, rated, and peak loads of the fire pump shall be determined by controlling the quantity of water discharged through approved test devices.

Exception: If available suction supplies do not permit the flowing of 150 percent of rated pump capacity, the fire pump shall be operated at maximum allowable discharge to determine its acceptance. This reduced capacity shall not constitute an unacceptable test.

11-2.6.3\* Measurement Procedure. The quantity of water discharging from the fire pump assembly shall be determined and stabilized. Immediately thereafter, the operating conditions of the fire pump and driver shall be measured.

11-2.6.3.1 For electric motors operating at rated voltage and frequency, the ampere demand shall not exceed the product of a full load ampere rating times the allowable service factor as stamped on the motor nameplate.

11-2.6.3.2 For electric motors operating under varying voltage, the product of the actual voltage and current demand shall not exceed the product of the rated voltage and rated full load current times the allowable service factor. The voltage at the motor shall not vary more than 5 percent below or 10 percent above rated (nameplate) voltage during the test. (See 6-3.1.2.)

- 11-2.6.3.3 Engine-driven units shall not show signs of overload or stress. The governor of such units shall be set at the time of the test to properly regulate the engine speed at rated pump speed. (See 8-2.4.1.)
- 11-2.6.3.4 The steam turbine shall maintain its speed within the limits as specified in 10-2.2.
- 11-2.6.3.5 The gear drive assembly shall operate without excessive objectionable noise, vibration, or heating.
- 11-2.6.4 Loads Start Test. The fire pump unit shall be started and brought up to rated speed without interruption under the conditions of a discharge equal to peak load.
- 11-2.6.5 Phase Reversal Test. For electric motors, a test shall be performed to ensure that there is not a phase reversal condition in either the normal power supply configuration or from the alternate power supply (where provided).

### 11-2.7 Controller Acceptance Test.

- 11-2.7.1\* Fire pump controllers shall be tested in accordance with the manufacturer's recommended test procedure. As a minimum, no less than six automatic and six manual operations shall be performed during the acceptance test.
- 11-2.7.2 A fire pump driver shall be operated for a period of at least 5 minutes at full speed during each of the above operations.
- Exception: An engine driver shall not be required to run for 5 minutes at full speed between successive starts until the cumulative cranking time of successive starts reaches 45 seconds.
- 11-2.7.3 The automatic operation sequence of the controller shall start the pump from all provided starting features. This shall include pressure switches or remote starting signals.
- 11-2.7.4 Tests of engine-drive controllers shall be divided between both sets of batteries.
- 11-2.7.5 The selection, size, and setting of all overcurrent protective devices (including fire pump controller circuit breaker) shall be confirmed to be in accordance with this standard.
- 11-2.7.6 Manual Emergency (Handle) Operation. The fire pump shall be started once from each power service and run for a minimum of 5 minutes.
  - CAUTION: Manual emergency operation is to be accomplished by a manual actuation of the emergency handle to the fully latched position in a continuous motion. The handle is to be latched for the duration of this test run.
- 11-2.8 Emergency Power Supply. On installations with an emergency source of power and an automatic transfer switch, loss of primary source shall be simulated and transfer shall occur while the pump is operating at peak load. Transfer from normal to alternate source and retransfer from alternate to normal source shall not cause opening of overcurrent protection devices in either line. At least half of the manual and automatic operations of 11-2.7.1 shall be performed with the fire pump connected to the alternate source.
- 11-2.8.1 If the alternate power source is a generator set required by 6-2.3.1, installation acceptance shall be in accordance with NFPA 110, Standard for Emergency and Standby Power Systems.

- 11-2.9 Emergency Governor. Emergency governor valve for steam shall be operated to demonstrate satisfactory performance of the assembly (hand tripping shall be acceptable).
- 11-2.10 Alarm conditions, both local and remote, shall be simulated to demonstrate satisfactory operation.
- 11-2.11 Test Duration. The fire pump shall be in operation for not less than 1 hour total time during all of the foregoing tests.

### 11-3 Manuals, Special Tools, and Spare Parts.

- 11-3.1 A minimum of one set of instruction manuals for all major components of the fire pump system shall be supplied by the manufacturer of each major component. The manual shall contain:
  - (a) A detailed explanation of the operation of the component,
  - (b) Instructions for routine maintenance,
  - (c) Detailed instructions concerning repairs,
  - (d) Parts list and parts identification, and
- (e) Schematic electrical drawings of controller, transfer switch, and alarm panels.
- 11-3.2 Any special tools and testing devices required for routine maintenance shall be available for inspection by the authority having jurisdiction at the time of the field acceptance test.
- 11-3.3 Consideration shall be given to stocking spare parts for critical items not readily available.
- 11-4 Periodic Inspection, Testing, and Maintenance. Fire pumps shall be inspected, tested, and maintained in accordance with NFPA 25, Standard for the Inspection, Testing, and Maintenance of Water-Based Fire Protection Systems.
- 11-5 Impeller Replacement. Whenever the impeller in a listed fire pump is replaced with an identical impeller or rotating assembly, a field re-test of the pump unit shall be performed. The re-test shall be conducted by the pump manufacturer, or designated representative, or pump qualified person who is so designated by the appropriate authorities. The field re-test results shall equal the original pump performance as indicated by the original factory-certified test curve, whenever it is available, and they shall be within the accuracy limits of field testing as stated elsewhere in this standard.

### **Chapter 12 Referenced Publications**

- 12-1 The following documents or portions thereof are referenced within this standard and shall be considered part of the requirements of this document. The edition indicated for each reference is the current edition as of the date of the NFPA issuance of this document.
- 12-1.1 NFPA Publications. National Fire Protection Association, 1 Batterymarch Park, P.O. Box 9101, Quincy, MA 02269-9101.
- NFPA 13, Standard for the Installation of Sprinkler Systems, 1996 edition.
- NFPA 24, Standard for the Installation of Private Fire Service Mains and Their Appurtenances, 1995 edition.
- NFPA 25, Standard for the Inspection, Testing, and Maintenance of Water-Based Fire Protection Systems, 1995 edition.

NFPA 37, Standard for the Installation and Use of Stationary Combustion Engines and Gas Turbines, 1994 edition.

NFPA 51B, Standard for Fire Prevention in Use of Cutting and Welding Processes, 1994 edition.

NFPA 70, National Electrical Code, 1996 edition.

NFPA 110, Standard for Emergency and Standby Power Systems, 1996 edition.

NFPA 1963, Standard for Fire Hose Connections, 1993 edition.

12-1.2 ANSI Publications. American National Standards Institute, 11 West 42nd Street, New York, NY 10036.

ANSI/IEEE C62.1-1989, IEEE Standard for Gapped Silicon-Carbide Surge Arresters for AC Power Circuits.

ANSI/IEEE C62.11-1987, IEEE Standard for Metal-Oxide Surge Arresters for AC Power Circuits.

NOTE: Arresters in ANSI/IEEE C62.11 are normally zinc-oxide without gaps.

ANSI/IEEE C62.41-1991, Recommended Practice for Surge Voltages in Low-Voltage AC Power Circuits.

#### 12-1.3 Other Codes and Standards.

Hydraulics Institute Standards for Centrifugal, Rotary and Reciprocating Pumps, 14th ed., Hydraulic Institutes, 1230 Keith Building, Cleveland, OH 44115, 1983.

NEMA Industrial Control and Systems Standards, ICS 2.2-83, *Maintenance of Motor Controllers After a Fault Condition*, and NEMA MG-1-1978, Parts 2 and 14, National Electrical Manufacturers Assn., 1300 N. 17th Street, Suite 1847, Rosslyn, VA 22209.

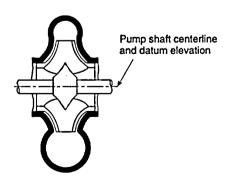
## Appendix A Explanatory Material

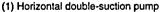
This Appendix is not a part of the requirements of this NFPA document, but is included for information purposes only.

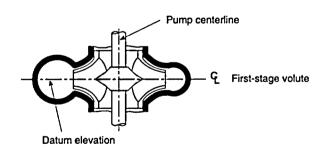
- **A-1-4** Because of the unique nature of fire pump units, the approval should be obtained prior to the assembly of any specific component.
- A-1-6.1 A single entity should be designated as having unit responsibility for the pump, driver, controller, transfer

switch equipment, and accessories. Unit responsibility means the accountability to answer and resolve any and all problems regarding the proper installation, compatibility, performance, and acceptance of the equipment. Unit responsibility should not be construed to mean purchase of all components from a single supplier.

- A-1-8 Approved. The National Fire Protection Association does not approve, inspect, or certify any installations, procedures, equipment, or materials; nor does it approve or evaluate testing laboratories. In determining the acceptability of installations, procedures, equipment, or materials, the authority having jurisdiction may base acceptance on compliance with NFPA or other appropriate standards. In the absence of such standards, said authority may require evidence of proper installation, procedure, or use. The authority having jurisdiction may also refer to the listings or labeling practices of an organization concerned with product evaluations that is in a position to determine compliance with appropriate standards for the current production of listed items.
- A-1-8 Authority Having Jurisdiction. The phrase "authority having jurisdiction" is used in NFPA documents in a broad manner, since jurisdictions and approval agencies vary, as do their responsibilities. Where public safety is primary, the authority having jurisdiction may be a federal, state, local, or other regional department or individual such as a fire chief; fire marshal; chief of a fire prevention bureau, labor department, or health department; building official; electrical inspector; or other's having statutory authority. For insurance purposes, an insurance inspection department, rating bureau, or other insurance company representative may be the authority having jurisdiction. In many circumstances, the property owner or his or her designated agent assumes the role of the authority having jurisdiction; at government installations, the commanding officer or departmental official may be the authority having jurisdiction.
- A-1-8 Head. Head is a quantity used to express a form (or combination of forms) of the energy content of water per unit weight of the water referred to any arbitrary datum. In terms of foot-pounds (m-kg) of energy per pound (kg) of water, all head quantities have the dimensions of feet (m) of water. All pressure readings are converted into feet (m) of the water being pumped. [See Figure A-1-8(a), parts (1) and (2).]







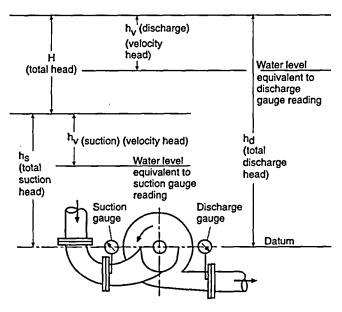
(2) Vertical double-suction pump

(1) For all types of horizontal shaft pumps (single-stage double-suction pump shown). Datum is same for multistage, single- (end) suction ANSI type or any pump with a horizontal shaft. (2) For all types of vertical shaft pumps (single-stage vertical double-suction pump shown). Datum is same for single- (end) suction, in line, or any pump with a vertical shaft.

Figure A-1-8(a) Datum elevation of various centrifugal pump designs.

A-1-8 Listed. The means for identifying listed equipment may vary for each organization concerned with product evaluation, some of which do not recognize equipment as listed unless it is also labeled. The authority having jurisdiction should utilize the system employed by the listing organization to identify a listed product.

A-1-8 Total Head (H), Horizontal Pumps. See Figure A-1-8(b).



Installation with suction head above atmospheric pressure shown

Figure A-1-8(b) Total head of all types of centrifugal (not vertical turbinetype) fire pumps. Pictorial does not show the various types of pumps applicable.

A-1-8 Total Head (H), Vertical Turbine Pumps. See Figure A-1-8(c).

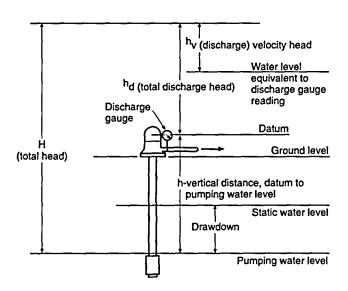


Figure A-1-8(c) Total head of vertical turbine-type fire pumps.

- A-2-1.1 For water supply capacity and pressure requirements, refer to:
  - (a) NFPA 13, Standard for the Installation of Sprinkler Systems.
- (b) NFPA 14, Standard for the Installation of Standpipe and Hose Systems.
- (c) NFPA 15, Standard for Water Spray Fixed Systems for Fire Protection.
- (d) NFPA 16, Standard for the Installation of Deluge Foam-Water Sprinkler and Foam-Water Spray Systems.
- (e) NFPA 24, Standard for the Installation of Private Fire Service Mains and Their Appurtenances.
- A-2-1.2 Where the suction supply is from a factory use water system, pump operation at 150 percent of rated capacity should not create hazardous process upsets due to low water pressure.
- A-2-1.4 Water sources containing salt or other materials deleterious to the fire protection systems should be avoided.
- A-2-3 A centrifugal fire pump should be selected in the range of operation from 90 percent to 150 percent of its rated capacity. The performance of the pump when applied at capacities over 140 percent of rated capacity may be adversely affected by the suction conditions. Application of the pump at capacities less than 90 percent of the rated capacity is not recommended.

The selection and application of the fire pump should not be confused with pump operating conditions. With proper suction conditions, the pump can operate at any point on its characteristic curve from shutoff to 150 percent of its rated capacity.

A-2-5.2 For protection against damage from overpressure, where desired, a gauge protector should be installed.

A-2-7 Special consideration needs to be given to fire pump installations installed below grade. Light, heat, drainage, and ventilation are several of the variables that need to be addressed. Some locations or installations may not require a pump house. Where a pump room or pump house is required, it should be of ample size and located to permit short and properly arranged piping. The suction piping should receive first consideration. The pump house should preferably be a detached building of noncombustible construction. A one-story pump room with a combustible roof, either detached or well cut off from an adjoining one-story building, is acceptable if sprinklered. Where a detached building is not feasible, the pump room should be so located and constructed as to protect the pump unit and controls from falling floors or machinery and from fire that might drive away the pump operator or damage the pump unit or controls. Access to the pump room should be provided from outside the building. Where the use of brick or reinforced concrete is not feasible, metal lath and plaster is recommended for the construction of the pump room. The pump room or pump house should not be used for storage purposes. Vertical shaft turbine-type pumps may require a removable panel in the pump house roof to permit the pump to be removed for inspection or repair. Proper clearances to equipment should be provided as recommended by the manufacturer's drawings.

**A-2-7.1 Impairment.** A fire pump that is inoperative for any reason at any time constitutes an impairment to the fire protection system. It should be returned to service without delay.

Rain and intense heat of the sun are adverse conditions to equipment not installed in a completely protective enclosure. At a minimum, equipment installed outdoors should be shielded by a roof or deck.

A-2-7.6 Pump rooms and pump houses should be dry and free of condensate. Some heat may be required to accomplish this.

A-2-8.1 The exterior of aboveground steel piping should be kept painted.

A-2-8.4 When welding on the pump suction or discharge piping with the pump in place, the welding ground should be on the same side of the pump as the welding.

**A-2-9.1** The exterior of steel suction piping should be kept painted.

Buried iron or steel pipe should be lined and coated or protected against corrosion in conformance with applicable AWWA (AWWA-C104) or equivalent standards.

## A-2-9.4 See Figure A-2-9.4.

NOTE 1: A jockey pump is usually required with automatically controlled pumps.

NOTE 2: If testing facilities are to be provided, also refer to Figures A-2-14.1.2(a) and (b).

NOTE 3: Pressure sensing lines also need to be installed in accordance with 7-5.2.1. See Figures A-7-5.2.1(a) and (b).

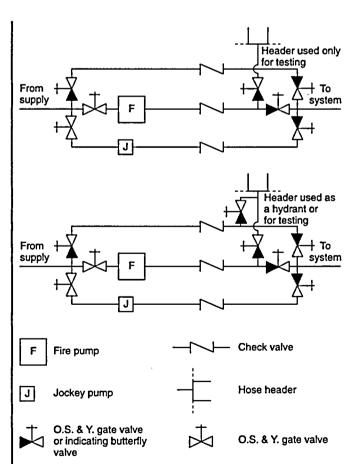


Figure A-2-9.4 Schematic diagram of suggested arrangements for a fire pump with a bypass, taking suction from public mains.

A-2-9.5 Where the suction supply is from public water mains, the gate valve should be located as far as is practical from the suction flange on the pump. Where it comes from a stored water container, the gate valve should be located at the outlet of the container. A butterfly valve on the suction side of the pump can create turbulence adversely affecting the pump performance and can increase the possibility of blockage of the pipe.

**A-2-9.6** See Figure A-2-9.6.

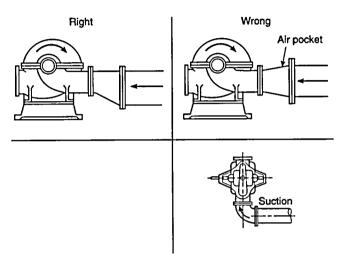


Figure A-2-9.6 Right and wrong pump suctions. (See Hydraulics Institute Standards for Centrifugal, Rotary and Reciprocating Pumps for additional information.)

A-2-9.8 When selecting screen material, consideration should be given to prevention of fouling from aquatic growth. This is best accomplished with brass or copper wire.

A-2-9.9 The term device as used in this section is intended to include, but not be limited to, devices that sense suction pressure and then restrict or stop the fire pump discharge. Due to the pressure losses and the potential for interruption of the flow to the fire protection systems, the use of backflow prevention devices is discouraged in fire pump piping. Where required, however, the placement of such a device on the discharge side of the pump is to ensure acceptable flow characteristics to the pump suction. It is more efficient to lose the pressure after the pump has boosted it, rather than before the pump has boosted it.

A-2-10.3 The discharge pipe size should be such that with the pump(s) operating at 150 percent of rated capacity the velocity in the discharge pipe does not exceed 20 ft/sec (6.2 m/s).

A-2-10.4 Large fire protection systems sometimes experience severe water hammer caused by back flow when the automatic control shuts down the fire pump. Where conditions may be expected to cause objectionable water hammer, a listed anti-water-hammer check valve should be installed in the discharge line of the fire pump. Automatically controlled pumps in tall buildings might give trouble from water hammer as the pump is shutting down.

**A-2-11** Isolation valves and control valves are considered to be identical when used in conjunction with a backflow prevention assembly.

A-2-12 Pipe breakage caused by movement can be greatly lessened and, in many cases, prevented by increasing flexibility between major parts of the piping. One part of the piping should never be held rigidly and another free to move, without provisions for relieving the strain. Flexibility can be provided by the use of flexible couplings at critical points and by allowing clearances at walls and floors. Fire pump suction and discharge pipes should be treated the same as sprinkler risers for whatever portion is within a building. (See NFPA 13, Standard for the Installation of Sprinkler Systems.)

Holes through pump room fire walls should be packed with mineral wool or other suitable material held in place by pipe collars on each side of the wall. Pipes passing through foundation walls or pit walls into ground should have clearance from these walls, but holes should be watertight. Space around pipes passing through pump room walls or pump house floors may be filled with asphalt mastic.

A-2-13.1 Pumps supplying only standpipe systems do not generally require relief valves.

A-2-13.5 The relief valve cone should be piped to a point where water can be freely discharged, preferably outside the building. If the relief valve discharge pipe is connected to an underground drain, care should be taken that no steam drains enter near enough to work back through the cone and into the pump room.

A-2-13.8 Where the relief valve discharges back to the source of supply, the back pressure capabilities and limitations of the valve to be used should be determined. It may be necessary to increase the size of the relief valve and piping above the minimum to obtain adequate relief capacity due to back pressure restriction.

A-2-13.9 When discharge enters the reservoir below minimum water level, there is not likely to be an air problem. If it enters over the top of the reservoir, the air problem is reduced by extending the discharge to below the normal water level.

A-2-14.1.2 Outlets can be provided through the use of standard test headers, yard hydrants, wall hydrants, or standpipe hose valves.

The following Notes apply to Figures A-2-14.1.2(a) and (b).

NOTE 1: Distance as recommended by the meter manufacturer.

NOTE 2: Distance not less than five diameters of suction pipe for top or bottom suction connection. Distance not less than ten diameters of suction pipe for side connection (not recommended).

NOTE 3: Automatic air release if piping forms an inverted "U," trapping air.

NOTE 4: The fire protection system should have outlets available to test the fire pump and suction supply piping. (See A-2-14.3.1.)

NOTE 5: The closed loop meter arrangement will only test net pump performance. It does not test the condition of the suction supply, valves, piping, etc.

NOTE 6: Return piping should be so arranged that no air can be trapped that would eventually end up in the eye of the pump impeller.

NOTE 7: Turbulence in the water entering the pump must be avoided to eliminate cavitation that would reduce pump discharge and damage the pump impeller. For this reason, side connection is not recommended.

NOTE 8: Prolonged recirculation can cause damaging heat buildup, unless some water is wasted.

NOTE 9: Flow meter must be installed according to manufacturer's instructions.

NOTE 10: Pressure sensing lines also need to be installed in accordance with 7-5.2.1. [See Figures A-7-5.2.1(a) and (b).]

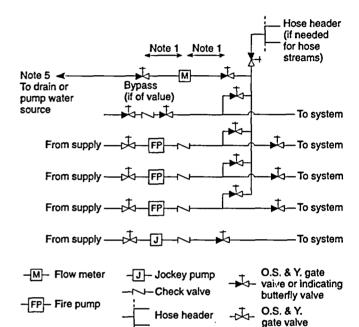


Figure A-2-14.1.2(a) Diagram of preferred arrangement for measuring fire pump water flow with meter for multiple pumps and water supplies, water discharge to drain or to pump water source.

#### A-2-14.2.1 Metering devices should discharge to drain.

Exception: In the case of a limited water supply, the discharge should be back to the water source (suction tank, small pond, etc.). If this discharge enters the source below minimum water level, it is not likely to create an air problem for the pump suction. If it enters over the top of the source, the air problem is reduced by extending the discharge to below the normal water level.

A-2-14.3.1 The hose valves should be attached to a header or manifold and connected by suitable piping to the pump discharge piping. The connection point should be between the discharge check valve and the discharge gate valve. Hose valves should be located to avoid any possible water damage to the pump driver or controller, and they should be outside the pump room or pump house. If there are other adequate pump testing facilities, the hose valve header may be omitted when its main function is to provide a method of pump and suction supply testing. Where the hose header also serves as the equivalent of a yard hydrant, this omission should not reduce the number of hose valves to less than two.

A-2-17 (a) Rotation of Pumps. Pumps are designated as having right-hand [or clockwise (CW)] rotation, or left-hand [or counterclockwise (CCW)] rotation. Diesel engines are commonly stocked and supplied with clockwise rotation.

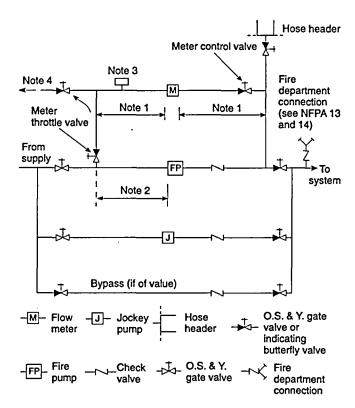


Figure A-2-14.1.2(b) Diagram of typical arrangement for measuring fire pump water flow with meter, discharge to pump suction.

(b) Horizontal Pump Shaft Rotation. The rotation of a horizontal pump can be determined by standing at the driver end and facing the pump. If the top of the shaft revolves from the left to the right, the rotation is right-hand [or clockwise (CW)]. If the top of the shaft revolves from right to left, the rotation is left-hand [or counterclockwise (CGW)].

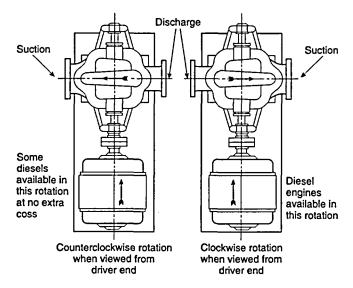


Figure A-2-17(b) Horizontal pump shaft rotation.

(c) Vertical Pump Shaft Rotation. The rotation of a vertical pump can be determined by looking down upon the top of the pump. If the point of the shaft directly opposite revolves

from left to right, the rotation is right-hand [or clockwise (CW)]. If the point of the shaft directly opposite revolves from right to left, the rotation is left-hand [or counterclockwise (CCW)].

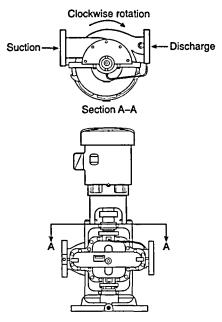


Figure A-2-17(c) Vertical pump shaft rotation.

A-2-18 In addition to those conditions that require alarm signals for pump controllers and engines, there are other conditions for which such alarms might be recommended, depending upon local conditions. Some of these supervisory alarm conditions are:

- (a) Low pump room temperature,
- (b) Relief valve discharge,
- (c) Flow meter left "on," bypassing the pump,
- (d) Water level in suction supply below normal,
- (e) Water level in suction supply near depletion,
- (f) Diesel fuel supply below normal,
- (g) Steam pressure below normal.

Such additional alarms may be incorporated into the trouble alarms already provided on the controller, or they may be independent.

A-2-19 Pressure maintenance (jockey or make-up) pumps should be used where it is desirable to maintain a uniform or relatively high pressure on the fire protection system. A jockey pump should be sized to make up the allowable leakage rate within 10 minutes or 1 gpm (3.8 L/min), whichever is larger.

**A-2-19.3** See Figure A-2-19.3.

**A-2-19.4** A centrifugal-type pressure maintenance pump is preferable.

NOTE 1: A jockey pump is usually required with automatically controlled pumps.

NOTE 2: Jockey pump suction may come from the tank filling supply line. This would allow high pressure to be maintained on the fire protection system even when the supply tank may be empty for repairs.

NOTE 3: Pressure sensing lines also need to be installed in accordance with 7-5.2.1. [See Figures A-7-5.2.1(a) and (b).]

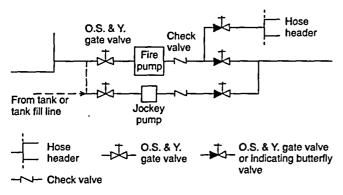


Figure A-2-19.3 Jockey pump installation with fire pump.

- | A-2-22.1 Paragraph 4-14.4.3 of NFPA 13, Standard for the Installation of Sprinkler Systems, contains specific guidance for seismic design of fire protection systems. Tables are available to determine the relative strength of many common bracing materials and fasteners.
- A-3-2.1 Listed pumps can have different head capacity curve shapes for a given rating. Figure A-3-2.1 illustrates the extremes of the curve shapes probable. Shutoff head will range from a minimum of 101 percent to a maximum of 140 percent of rated head. At 150 percent of rated capacity, head will range from a minimum of 65 percent to a maximum of just below rated head. Pump manufacturers can supply expected curves for their listed pumps.

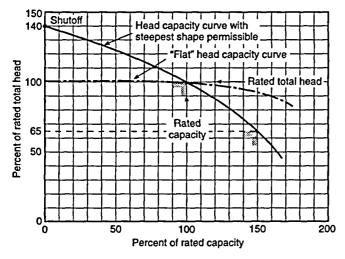
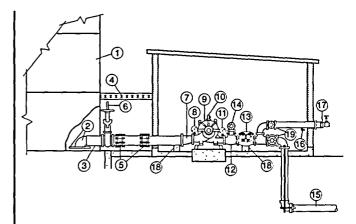


Figure A-3-2.1 Pump characteristics curves.

## **A-3-3.1** See Figure A-3-3.1.

- **A-3-4.1** Flexible couplings are used to compensate for temperature changes and to permit end movement of the connected shafts without interfering with each other.
- A-3-4.3 A substantial foundation is important in maintaining alignment. The foundation preferably should be made of reinforced concrete.
- A-3-5 If pumps and drivers were shipped from the factory with both machines mounted on a common base plate, they were accurately aligned before shipment. All base plates are



- 1. Aboveground suction tank
- Entrance elbow and square steel vortex plate with dimensions at least twice the diameter of the suction pipe. Distance above the bottom of tank is one-half the diameter of the suction pipe with minimum of 6 in. (152 mm).
- 3. Suction pipe
- 4. Frostproof casing
- 5. Flexible couplings for strain relief
- 6. O.S. & Y. gate valve (see 2-9.5 and A-2-9.5)
- 7. Eccentric reducer
- 8. Suction gauge

- 9. Horizontal split-case fire pump
- 10. Automatic air release
- 11. Discharge gauge
- 12. Reducing discharge tee
- 13. Discharge check valve14. Relief valve (if required)
- Supply pipe for fire protection system
- 16. Drain valve or ball drip
- 17. Hose valve manifold with hose valves
- 18. Pipe supports
- Indicating gate or Indicating butterfly valve

Figure A-3-3.1 Horizontal split-case fire pump installation with water supply under a positive head.

flexible to some extent and, therefore, must not be relied upon to maintain the factory alignment. Realignment is necessary after the complete unit has been leveled on the foundation and again after the grout has set and foundation bolts have been tightened. The alignment should be checked after the unit is piped and rechecked periodically. To facilitate accurate field alignment, most manufacturers either do not dowel the pumps or drivers on the base plates before shipment, or at most dowel the pump only.

After the pump and driver unit has been placed on the foundation, the coupling halves should be disconnected. The coupling should not be reconnected until the alignment operations have been completed.

The purpose of the flexible coupling is to compensate for temperature changes and to permit end movement of the shafts without interference with each other while transmitting power from the driver to the pump.

There are two forms of misalignment between the pump shaft and the driver shaft, as follows:

- (a) Angular Misalignment. Shafts with axes concentric but not parallel.
- (b) Parallel Misalignment. Shafts with axes parallel but not concentric.

The faces of the coupling halves should be spaced within the manufacturer's recommendations and far enough apart so that they cannot strike each other when the driver rotor is moved hard over toward the pump. Due allowance should be made for wear of the thrust bearings. The necessary tools for an approximate check of the alignment of a flexible coupling are a straight edge and a taper gauge or a set of feeler gauges.

A check for angular alignment is made by inserting the taper gauge or feelers at four points between the coupling faces and comparing the distance between the faces at four points spaced at 90-degree intervals around the coupling. The unit will be in angular alignment when the measurements show that the coupling faces are the same distance apart at all points.

A check for parallel alignment is made by placing a straight edge across both coupling rims at the top, bottom, and at both sides. The unit will be in parallel alignment when the straight edge rests evenly on the coupling rim at all positions. Allowance may be necessary for temperature changes and for coupling halves that are not of the same outside diameter. Care must be taken to have the straight edge parallel to the axes of the shafts.

Angular and parallel misalignment are corrected by means of shims under the motor mounting feet. After each change, it is necessary to recheck the alignment of the coupling halves. Adjustment in one direction may disturb adjustments already made in another direction. It should not be necessary to adjust the shims under the pump.

The permissible amount of misalignment will vary with the type of pump and driver; and coupling manufacturer, model, and size.

The best method for putting the coupling halves in final accurate alignment is by the use of a dial indicator.

When the alignment is correct, the foundation bolts should be tightened evenly but not too firmly. The unit can then be grouted to the foundation. The base plate should be completely filled with grout, and it is desirable to grout the leveling pieces, shims, or wedges in place. Foundation bolts should not be fully tightened until the grout is hardened, usually about 48 hours after pouring.

After the grout has set and the foundation bolts have been properly tightened, the unit should be checked for parallel and angular alignment, and, if necessary, corrective measures taken. After the piping of the unit has been connected, the alignment should be checked again.

The direction of driver rotation should be checked to make certain that it matches that of the pump. The corresponding direction of rotation of the pump is indicated by a direction arrow on the pump casing.

The coupling halves can then be reconnected. With the pump properly primed, the unit then should be operated under normal operating conditions until temperatures have stabilized. It then should be shut down and immediately checked again for alignment of the coupling. All alignment checks must be made with the coupling halves disconnected and again after they are reconnected.

After the unit has been in operation for about 10 hours or three months, the coupling halves should be given a final check for misalignment caused by pipe or temperature strains. If the alignment is correct, both pump and driver should be dowelled to the base plate. Dowel location is very important and the manufacturer's instructions should be obtained, especially if the unit is subjected to temperature changes.

The unit should be checked periodically for alignment. If the unit does not stay in line after being properly installed, the following are possible causes:

- (a) Settling, seasoning, or springing of the foundation. Pipe strains distorting or shifting the machine.
  - (b) Wear of the bearings.

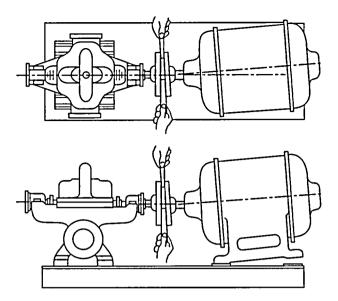


Figure A-3-5(a) Checking angular alignment.

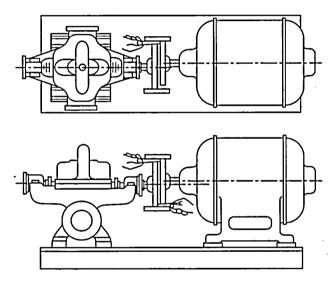


Figure A-3-5(b) Checking parallel alignment.1

- (c) Springing of the base plate by heat from an adjacent steam pipe or from a steam turbine.
- (d) Shifting of the building structure due to variable loading or other causes.

It may be necessary to slightly readjust the alignment from time to time, while the unit and foundation are new.

A-4-1 Supervision of Installation. Satisfactory operation of vertical turbine-type pumps is dependent to a large extent upon careful and correct installation of the unit; therefore, it is recommended that this work be done under the direction of a representative of the pump manufacturer.

<sup>&</sup>lt;sup>1</sup>Diagrams reprinted from Hydraulics Institute Standards for Centrifugal, Rotary and Reciprocating Pumps. (See Appendix C, Referenced Publications.)

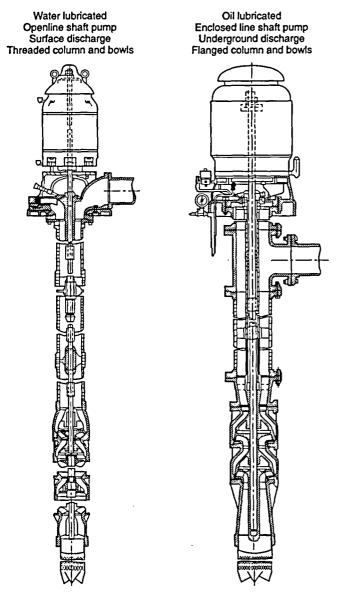


Figure A-4-1.1 Illustration of water-lubricated and oil-lubricated shaft pumps.

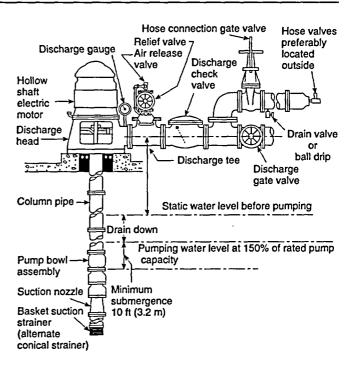
## **A-4-1.1** See Figure A-4-1.1.

A-4-2.1.1 Water Supply Source. Stored water supplies from reservoirs or tanks supplying wet pits are preferable. Lakes, streams, and groundwater supplies are acceptable where investigation shows that they can be expected to provide a suitable and reliable supply.

A-4-2.1.2 Aquifer Performance Analysis. The authority having jurisdiction may require an aquifer performance analysis. The history of the water table should be carefully investigated. The number of wells already in use in the area and the probable number that may be in use should be considered in relation to the total amount of water available for fire protection purposes.

## **A-4-2.2.1** See Figure A-4-2.2.1.

A-4-2.2.2 Intake Design. The velocities in the approach channel or intake pipe should not exceed approximately 2 ft/sec (0.7 m/s), and the velocity in the wetted pit should not exceed approximately 1 ft/sec (0.3 m/s).



Note: The distance between the bottom of the strainer and the bottom of the wet pit should be one-half of the pump bowl diameter but not less than 12 in. (305 mm).

Figure A-4-2.2.1 Vertical shaft turbine-type pump installation in a well.

The ideal approach is a straight channel coming directly to the pump. Turns and obstructions are detrimental since they may cause eddy currents and tend to initiate deepcored vortices. The amount of submergence for successful operation will depend greatly on the approaches of the intake and the size of the pump.

The Hydraulics Institute Standards for Centrifugal, Rotary and Reciprocating Pumps has recommended sump dimensions for flows 3000 gpm (11,355 L/min) and larger. The design of sumps for pumps with discharge capacities less than 3000 gpm (11,355 L/min) should be guided by the same general principles as shown in the Hydraulics Institute Standards for Centrifugal, Rotary and Reciprocating Pumps.

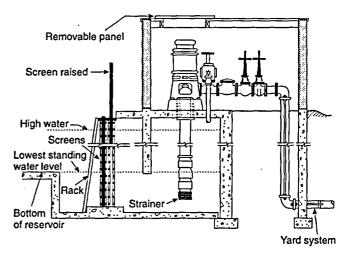
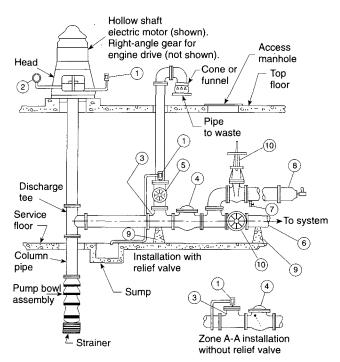


Figure A-4-2.2.2 Vertical shaft turbine-type pump installation in a wet pit.

**A-4-2.5 Consolidated Formations.** Where wells take their supply from consolidated formations such as rock, the specifications for the well should be decided upon by the authority having jurisdiction after consultation with a recognized groundwater consultant in the area.

**A-4-2.7 Test and Inspection of Well.** Before the permanent pump is ordered, the water from the well should be analyzed for corrosiveness, including such items as pH, salts such as chlorides, and harmful gases such as carbon dioxide  $(CO_2)$  or hydrogen sulfide  $(H_2S)$ . If the water is corrosive, the pumps should be constructed of a suitable corrosion-resistant material or covered with special protective coatings in accordance with the manufacturer's recommendations.

## **A-4-3.1** See Figure A-4-3.1.



- 1. Automatic air release
- 2. Discharge gauge
- 3 Reducing discharge tee
- 4. Discharge check valve
- 5. Relief valve (if required)
- 6. Discharge pipe
- 7. Drain valve or ball drip
- 8. Hose valve manifold with hose valves
- Pipe supports
- 10. Indicating gate or indicating butterfly

Figure A-4-3.1 Belowground discharge arrangement.

### A-4-3.5.3 Air Line Method of Water Level Detection.

- (a) A satisfactory method of determining the water level involves the use of an air line of small pipe or tubing and of known vertical length, a pressure or depth gauge, and an ordinary bicycle or automobile pump installed as shown in Figure A-4-3.5.3. The air line pipe should be of known length and extend beyond the lowest anticipated water level in the well in order to ensure more reliable gauge readings, and should be properly installed. As noted in Figure A-4-3.5.3, an air pressure gauge is used to indicate the pressure in the air line.
- (b) The air line pipe is lowered into the well, a tee is placed in the line above the ground, and a pressure gauge is screwed into one connection. The other connection is fitted with an

ordinary bicycle valve to which a bicycle pump is attached. All joints must be made carefully and must be airtight to obtain correct information. When air is forced into the line by means of the bicycle pump, the gauge pressure increases until all of the water has been expelled. When this point is reached, the gauge reading becomes constant. The maximum maintained air pressure recorded by the gauge is equivalent to that necessary to support a column of water of the same height as that forced out of the air line. The length of this water column is equal to the amount of air line submerged.

(c) Deducting this pressure converted to ft (m) (psi pressure  $\times$  2.31 = ft, and bars pressure  $\times$  10.3 = m) from the known length of the air line will give the amount of submergence.

*Example:* The following calculation will serve to clarify Figure A-4-3.5.3.

Assume a length (L) of 50 ft (15.2 m).

Pressure gauge reading before starting fire pump  $(p_1)$  = 10 psi (0.68 bars). Then  $A = 10 \times 2.31 = 23.1$  ft (0.68  $\times$  10.3 = 7.0 m); therefore, the water level in the well before starting the pump would be B = L - A = 50 ft - 23.1 ft = 26.9 ft (B = L - A = 15.2 m - 7 m = 8.2 m).

Pressure gauge reading when pumping  $(p_2) = 8$  psi (0.55 bars). Then  $C = 8 \times 2.31 = 18.5$  ft  $(0.55 \times 10.3 = 5.6 \text{ m})$ ; therefore, the water level in the well while pumping would be D = L - C = 50 ft - 18.5 ft = 31.5 ft (D = L - C = 15.2 m - 5.6 m = 9.6 m).

The drawdown may be determined by any of the following methods:

- (a) D B = 31.5 ft 26.9 ft = 4.6 ft (9.6 m 8.2 m = 1.4 m),
- (b) A C = 23.1 ft 18.5 ft = 4.6 ft (7.0 m 5.6 m = 1.4 m), or
- (c)  $p_1 p_2 = 10 8 = 2 \text{ psi} = 2 2.31 4.6 \text{ ft} (0.68 0.55 = 0.13 \text{ bars} = 0.13 10.3 = 1.4 \text{ m}).$
- **A-4-4 Method of Erecting.** Several methods of installing a vertical pump may be followed, depending upon the location of the well and facilities available. Since most of the unit is underground, extreme care must be used in assembling and installing it and in thoroughly checking the work as it progresses. The following simple method is the most common:
- (a) Construct a tripod or portable derrick and use two sets of installing clamps over the open well or pump house. After the derrick is in place, the alignment should be checked carefully with the well or wet pit to avoid any trouble when setting the pump.
- (b) Attach the set of clamps to the suction pipe on which the strainer has already been placed and lower into the well until clamps rest on a block beside the well casing or on the pump foundation.
- (c) Attach the clamps to the pump stage assembly, bring over the well, and install pump stages to the suction pipe, until each piece has been installed in accordance with the manufacturer's instructions.
- **A-4-7.1.1 Setting Impellers.** The setting of the impellers should be undertaken only by a representative of the pump manufacturer. Improper setting will develop excessive friction loss by rubbing of impellers on pump seals with resultant increase in power demand. If the impellers are adjusted too high, there will be a loss in capacity; and full capacity is vital for fire pump service. The top shaft nut should be locked or pinned after proper setting.

**20–4**3

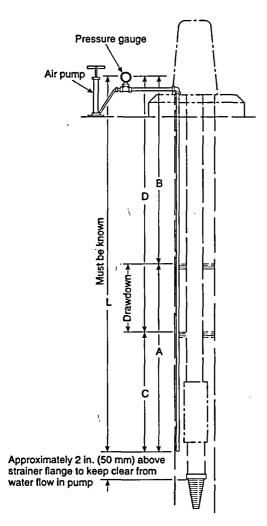


Figure A-4-3.5.5 Air line method of determining depth of water level.

A-4-7.1.2 Vibration and Excessive Motor Temperature. Pumping units are checked at the factory for smoothness of performance and should operate satisfactorily on the job. If excessive vibration is present, the following conditions may be causing the trouble: a bent pump or column shaft, impellers not properly set within the pump bowls, pump not hanging freely in the well, or strain transmitted through the discharge piping. Excessive motor temperature is generally caused either by a maintained low voltage of the electric service or by improper setting of impellers within the pump bowls.

A-6-2.2 A private generating plant located on the premises served by the fire pump is considered as a power station if it is in a separate power house or cut off from the main buildings. It may be used as one of the two sources of current supply. Where two sources are used with power transfer switches, refer to NFPA 70, National Electrical Code, Article 695.

## A-6-2.3 A reliable source possesses the following characteristics:

(a) Infrequent power disruptions from environmental or man-made conditions,

- (b) A separate service connection or connection to the supply side of the service disconnect, and
- (c) Service and feeder conductors either buried under 2 in. (50 mm) of concrete or encased in 2 in. (50 mm) of concrete or brick within a building.

Typical methods of routing power from the source to the motor are shown in Figure A-6-3.2.2. Other configurations may also be acceptable.

A-6-3 Where risks involved are large and interruption of fire pump service would seriously affect protection, at least two separate circuits from the power plant(s) to the pump room should be provided. The circuits should be run by separate routes or in such a manner that failure of more than one at the same time would be only a remote possibility.

A completely underground circuit from generating station to the pump room is strongly recommended and should be obtained where practicable. Where such construction is not available, an overhead circuit may be allowed, but that part of the circuit adjacent to the plant served by the fire pump or to exposing plants should be run with special reference to damage in case of fire. Where the pump room is part of, or in close proximity to, the plant that the pump is designed to protect, the wires should be underground for some distance from the pump room.

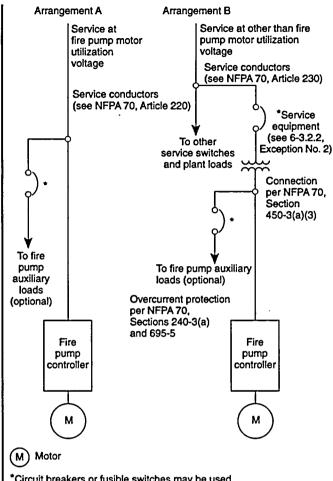
A-6-3.1.1 Under premise fire conditions, service and feeder connections are susceptible to failure from collapsing structural and other members within the premise as well as failure from fire. Under fire conditions generated by overcurrent within these service and feeder conductors, the characteristics of 6-3.1.1 minimize the possibility of fire spread.

Typical methods of routing power from the source to the motor are shown in Figure A-6-3.2.2. Other configurations may also be acceptable.

A-6-3.1.2 Normally, conductor sizing is based on appropriate Sections of NFPA 70, National Electrical Code, Article 430, except larger sizes might be required to meet the requirements of NFPA 70 695-8(e) (NFPA 20, 6-3.1.2). Transformer sizing is to be in accordance with NFPA 70, 695-5(a), except larger minimum sizes might be required to meet the requirements of NFPA 70, 695-8(e) (NFPA 20, 6-3.1.2).

A-6-3.2.2 Where the alternate power is from an on-site generator, the alternate service equipment need not be located in the fire pump room.

The Committee considered the potential arrangement of providing fire pump power from the secondary side of the transformer, which supplies other electrical loads of the facility. The Committee recognizes that it is possible to supply the fire pump power ahead of other plant loads and to protect the fire pump power circuit by proper electrical coordination. However, the Committee is concerned that, while responding to an emergency, fire fighters may seek to disconnect electrical power to the facility by opening the transformer primary disconnect, which in this case would isolate power to the fire pump as well. In addition, the Committee is concerned that the designed electrical coordination may be compromised by ongoing additional electrical loads to the facility power distribution system. Therefore, if electrical service is supplied to the facility at voltage higher than utilization voltage, the Committee feels that a separate transformer to provide power to the fire pump is appropriate.



\*Circuit breakers or fusible switches may be used

Figure A-6-3.2.2 Typical power supply arrangements from source to motor.

- A-6-6.3 Where a generator is installed to supply power to loads in addition to one or more fire pump drivers, the fuel supply should be sized to provide adequate fuel for all connected loads for the desired duration. The connected loads can include such loads as emergency lighting, exit signage, and elevators.
- A-7-1.1.2 "Suitable for use" means that the controller and transfer switch have been prototype tested and have demonstrated by these tests their short-circuit withstandability and interrupting capacity at the stated magnitude of short-circuit current and voltage available at their line terminals (see ANSI/UL 509 and ANSI/UL 1008).

A short-circuit study should be made to establish the available short-circuit current at the controller in accordance with IEEE 141, Electric Power Distribution for Industrial Plants; IEEE 241, Electric Systems for Commercial Buildings; or other acceptable methods.

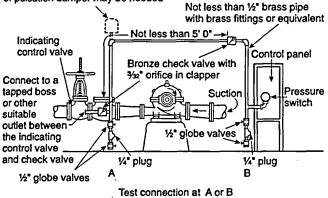
After the controller and transfer switch have been subjected to a high fault current, they may not be suitable for further use without inspection or repair. Refer to National Electrical Manufacturers Association Part ICS 2.2-1983, Maintenance of Motor Controllers After a Fault Condition.

- A-7-2.1 If the controller must be located outside of the pump room, a glazed opening should be provided in the pump room wall for observation of the motor and pump during starting. The pressure control pipe line should be protected against freezing and mechanical injury.
- A-7-3.7.3 Pump operators should be familiar with instructions provided for controllers and should observe in detail all of their recommendations.
- A-7-4.1 Operation of the surge arrester should not cause either the isolating switch or the circuit breaker to open.
- A-7-4.3.3 Attention should be given to the type of service grounding to establish circuit breaker interrupting rating based on grounding type employed.
- A-7-4.3.3(d) The interrupting rating may be less than the suitability rating where other devices within the controller assist in the current-interrupting process.
- A-7-4.3.3(f) Exception. Current limiters are melting linktype devices that, where used as an integral part of a circuit breaker, limit the current during a short circuit to within the interrupting capacity of the circuit breaker.
- A-7-4.6 The pilot lamp for alarm and signal service should have operating voltage less than the rated voltage of the lamp to ensure long operating life. When necessary, a suitable resistor or potential transformer should be used to reduce the voltage for operating the lamp.
- A-7-4.7(b) To supervise the power source for the alarm circuit, the controller may be arranged to start upon failure of the alarm circuit power.
- A-7-5.1 The following definitions are derived from NFPA 70, National Electrical Code:
- 'Automatic. Self-acting, operating by its own mechanism when actuated by some impersonal influence, as for example, a change in current strength, pressure, temperature, or mechanical configuration.

Nonautomatic. The implied action requires personal intervention for its control. As applied to an electric controller, nonautomatic control does not necessarily imply a manual controller, but only that personal intervention is necessary.

- A-7-5.2.1 Installation of the pressure-sensing line in between the discharge check valve and the control valve is necessary to facilitate isolation of the jockey pump controller (and sensing line) for maintenance without having to drain the entire system. [See Figures A-7-5.2.1(a) and (b).]
- A-7-6.1 Voltages in excess of 600 volts are not recommended for fire pump service. Where it is impracticable to use a low voltage, higher voltages may be accepted.
- A-7-7 The authority having jurisdiction may permit the use of a limited-service controller for special situations where such use is acceptable to said authority.
- A-7-8 Typical fire pump controller and transfer switch arrangements are as shown in Figure A-7-8. Other configurations may also be acceptable.
- A-7-8.2 The compartmentalization or separation is to prevent propagation of a fault in one compartment to the source in the other compartment.

If water pulsation causes erratic operation of the pressure switch or the recorder, a supplemental air chamber or pulsation damper may be needed

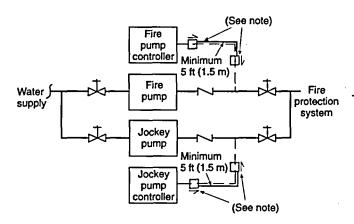


If water is clean, ground-face unions with noncorrosive diaphragms drilled for 1/20" orifices may be used in place of the check valves.

For SI units: 1 in. = 25.4 mm; 1 ft = 0.3048 m.

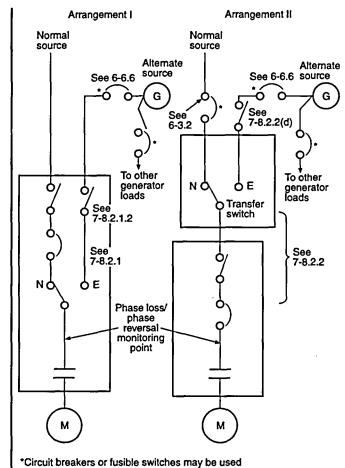
Note: Solenoid drain valve used for engine-driven fire pumps may be at A, B, or inside of controller enclosure.

Figure A-7-5.2.1(a) Piping connection for each automatic pressure switch (for fire pump and jockey pumps).



Note: Check valves or ground-face unions complying with 7-5.2.1.

Figure A-7-5.2.1(b) Piping connection for pressure-sensing line.

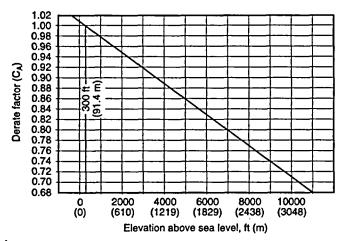


O. . . . O. .

(M) Motor (G) Generator

Figure A-7-8 Typical fire pump controller and transfer switch arrangements.

#### A-8-2.2.4 See Figure A-8-2.2.4.

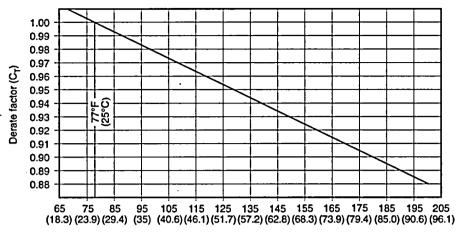


Note: Correction equation:

Corrected engine horsepower =  $(C_A + C_T - 1) \times Listed$  engine horsepower

 $C_A$  = Derate factor for elevation  $C_T$  = Derate factor for temperature

Figure A-8-2,2.4 Elevation derate curve.



Ambient air temperature at engine inlet, °F (°C)

Note: Correction equation: Corrected engine horsepower =  $(C_A + C_T - 1) \times L$ isted engine horsepower

 $C_A$  = Derate factor for elevation  $C_T$  = Derate factor for temperature

Figure A-8-2.2.5 Temperature derate curve.

A-8-2.2.5 Pump room temperature rise should be considered when determining the maximum ambient temperature specified.

A-8-2.4.7 This is to ensure ready wiring in the field between the two sets of terminals.

A-8-2.4.8 Terminations should be made using insulated ring-type compression connectors for post-type terminal blocks. Saddle-type terminal blocks should have the wire stripped with about  $\frac{1}{16}$  in. (1.6 mm) of bare wire showing after insertion in the saddle to ensure that no insulation is below the saddle. Wires should be tugged to ensure adequate tightness of the termination.

A-8-2.4.9 Manual mechanical operation of the main battery contactor will bypass all of the control circuit wiring within the controller.

**A-8-2.5.2.3** A single charger that automatically alternates from one battery to another may be used on two battery installations.

A-8-2.5.2.5 Location at the side of and level with the engine is recommended to minimize lead length from battery to starter.

**A-8-2.5.4.4** Automatic maintenance of air pressure is preferable.

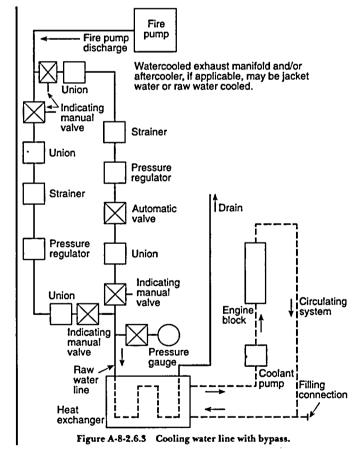
**A-8-2.6.3** See Figure A-8-2.6.3.

A-8-2.6.4 Where the water supply can be expected to contain foreign materials such as wood chips, leaves, lint, etc., the strainers required in 8-2.6.3 should be of the duplex filter type. Each filter (clean) element should be of sufficient filtering capacity to permit full water flow for a 3-hour period. In addition, a duplex filter of the same size should be installed in the bypass line. (See Figure A-8-2.6.3.)

A-8-3 The engine-driven pump may be located in a pump house or in a pump room that should be entirely cut off from the main structure by noncombustible construction.

A-8-3.2 For optimum room ventilation, the air supply ventilator and air discharge should be located on opposite walls.

When calculating the maximum temperature of the pump room, the radiated heat from the engine, the radiated



heat from the exhaust piping, and all other heatcontributing sources should be considered.

If the pump room is to be ventilated by a power ventilator, reliability of the power source during a fire should be considered. If the power source is unreliable, the temperature rise calculation should assume the ventilator is not operable.

Air consumed by the engine for combustion should be considered as part of the air changes in the room.

Pump rooms with heat-exchanger-cooled engines will typically require more air changes than engine air consumption will provide. To control the temperature rise of the room, additional air flow through the room is normally required.

Pump rooms with radiator-cooled engines might have sufficient air changes due to the radiator discharge and engine consumption.

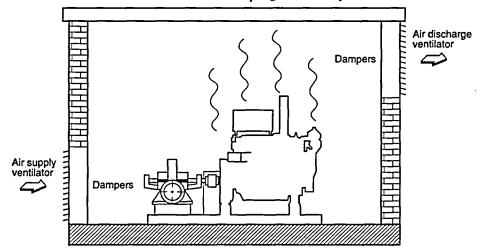
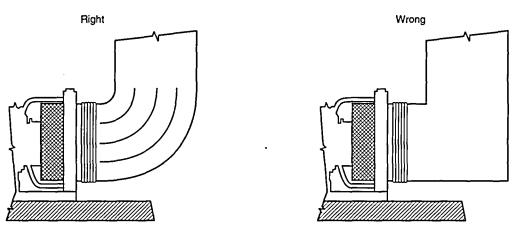


Figure A-8-3.2(a) Typical ventilation system for a heat-exchanger-cooled diesel-driven pump.



If a bend in the ducting cannot be avoided, it should be radiused and should include turning vanes to prevent turbulence and flow restriction.

This configuration should not be used, turbulence will not allow adequate air flow.

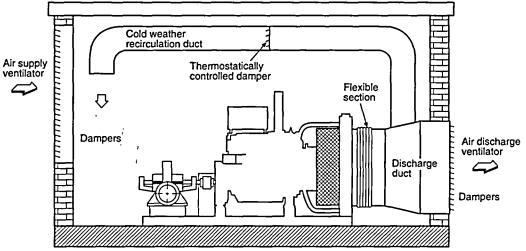


Figure A-8-3.2(b) Typical ventilation system for a radiator-cooled diesel-driven pump.

A-8-3.2.1 When motor-operated dampers are used in the air supply path, they should be spring operated to the open position and motored closed. Motor-operated dampers should be signaled to open when or before the engine begins cranking to start.

The maximum air flow restriction limit for the air supply ventilator is necessary to be compatible with listed engines to ensure adequate air flow for cooling and combustion. This restriction will typically include: louvers, bird screen, dampers, duct, or anything in the air supply path between the pump room and the outdoors.

Motor-operated dampers are recommended for the heatexchanger-cooled engines to enhance convection circulation.

Gravity-operated dampers are recommended for use with radiator-cooled engines to simplify their coordination with the air flow of the fan.

A-8-3.2.2 When motor-operated dampers are used in the air discharge path, they should be spring operated to the open position, motored closed, and be signaled to open when or before the engine begins cranking to start.

Prevailing winds can work against the air discharge ventilator. Therefore, the winds should be considered when determining the location for the air discharge ventilator. See Figure A-8-3.2.2 for the recommended wind wall design.

For heat-exchanger-cooled engines, an air discharge ventilator with motor-driven dampers, designed for convection circulation is preferred in lieu of a power ventilator. This arrangement will require the size of the ventilator to be larger, but it is not dependent on a power source that might not be available during the pump operation.

For radiator-cooled engines, gravity-operated dampers are recommended. Louvers and motor-operated dampers are not recommended due to the restriction to air flow they create and the air pressure they must operate against.

The maximum air flow restriction limit for the airdischarge ventilator is necessary to be compatible with listed engines to ensure adequate air-flow cooling.

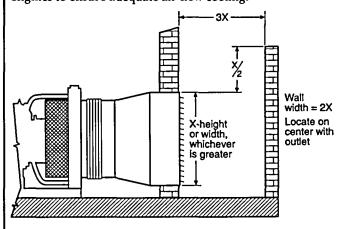


Figure A-8-3.2.2 Typical wind wall.

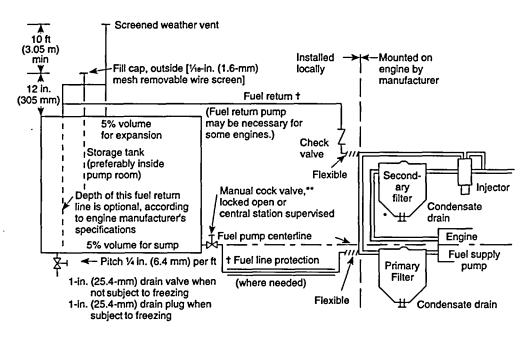
- A-8-4.3 One gal per horsepower (5.07 L/kW) is equivalent to 1 pint per horsepower (0.473 L/kW) per hour for 8 hours. Where prompt replenishment of fuel supply is unlikely, a reserve supply should be provided along with facilities for transfer to the main tanks.
- A-8-4.5 Diesel fuel storage tanks should be located preferably inside the pump room or pump house, if permitted by local regulations. Fill and vent lines in such case should be extended to outdoors. The fill pipe may be used for a gauging well where practical.

- A-8-4.6 NFPA 31, Standard for the Installation of Oil-Burning Equipment, may be used as a guide for diesel fuel piping. Figure A-8-4.6 shows a suggested diesel engine fuel system.
- A-8-4.7 The pour point and cloud point should be at least 10°F (5.6°C) below the lowest expected fuel temperature (see 2-7.3 and 8-4.5).
- A-8-5.3 A conservative guideline is that, if the exhaust system exceeds 15 ft (4.5 m) in length, the pipe size should be increased one pipe size larger than the engine exhaust outlet size for each 5 ft (1.5 m) in added length.
- A-8-6 Internal combustion engines necessarily embody moving parts of such design and in such number that the engines cannot give reliable service unless given intelligent care. The manufacturer's instruction book covering care and operation should be readily available, and pump operators should be familiar with its contents. All of its provisions should be observed in detail.
- A-8-6.5 Proper engine temperature when the engine is not running may be maintained through the circulation of hot water through the jacket or through heating of engine water by electric elements inserted into the block. As a general rule, water heaters and oil heaters are required for diesel engines below 70°F (21°C). The benefits to be gained are as follows:
- (a) Quick starting (fire pump engines may have to carry full load as soon as started),
  - (b) Reduced engine wear,
  - (c) Reduced drain on batteries,
  - (d) Reduced oil dilution, and
- (e) Reduced carbon deposits, so that the engine is far more likely to start every time.
- A-9-2.1 If the controller must be located outside of the pump room, a glazed opening should be provided in the pump room wall for observation of the motor and pump during starting. The pressure control pipe line should be protected against freezing and mechanical injury.
- A-9-3.1 In areas affected by excessive moisture, heat may be useful in reducing the dampness.
- A-9-3.8 Pump operators should be familiar with instructions provided for controllers and should observe in detail all of their recommendations.
- A-9-4.1.2 It is recommended that the pilot lamp for alarm and signal service have operating voltage less than the rated voltage of the lamp to ensure long operating life. When necessary, a suitable resistor should be used to reduce the voltage for operating the lamp.

## A-9-4.2(c) Trouble Signals.

- (a) A common signal may be used for the following trouble indications: items in 9-4.1.3(a), (b), (c), (d), and (e) and loss of output of battery charger on the load side of the dc overcurrent protective device.
- (b) If there is no other way to supervise loss of power, the controller may be equipped with a power failure circuit, which should be time delayed to start the engine upon loss of current output of the battery charger.
- A-9-5 NFPA 70, National Electrical Code, provides related definitions:

Automatic. Self-acting, operating by its own mechanism when actuated by some impersonal influence, as for example, a change in current strength, pressure, temperature, or mechanical configuration.



- Secondary filter behind or before engine fuel pump, according to engine manufacturer's specifications.
- \*\* Excess fuel may be returned to fuel supply pump suction, if recommended by engine manufacturer.
- † Size of fuel piping, according to engine manufacturer's specifications.

Figure A-8-4.6 Fuel system for diesel-engine-driven fire pump.

Nonautomatic. The implied action requires personal intervention for its control. As applied to an electric controller, nonautomatic control does not necessarily imply a manual controller, but only that personal intervention is necessary.

A-9-5.4.2 Manual shutdown of fire pumps is preferred. Automatic fire pump shutdown can occur during an actual fire condition when relatively low flow conditions signal the controller that pressure requirements have been satisfied.

**A-10-1.3** Single-stage turbines of maximum reliability and simplicity are recommended where the available steam supply will permit.

### A-10-2 Automatically Controlled Turbines.

#### A-10-2.1.1 The casing may be of cast iron.

Some applications may require a turbine-driven fire pump to start automatically, but not require the turbine to be on pressure control after starting. In such cases a satisfactory quickopening manual-reset valve installed in a bypass of the steam feeder line around a manual control valve may be used.

Where the application requires the pump unit to start automatically and after starting continue to operate by means of a pressure signal, the use of a satisfactory pilot-type pressure control valve is recommended. This valve should be located in the bypass around the manual control valve in the steam feeder line. The turbine governor control valve, when set at approximately 5 percent above the normal full-load speed of the pump under automatic control, would act as a preemergency control.

In the arrangements set forth in the two preceding paragraphs, the automatic valve should be located in the bypass around the manual control valve, which would normally be kept in the closed position. In the event of failure of the automatic valve, this manual valve could be opened, allowing the turbine to come to speed and be controlled by the turbine governor control valve(s).

The use of a direct-acting pressure regulator operating on the control valve(s) of a steam turbine is not recommended.

#### A-10-3 Installation Data.

- (a) The steam supply for the fire pump should preferably be an independent line from the boilers. It should be run so as to not be liable to injury in case of fire in any part of the property. The other steam lines from the boilers should be controlled by valves located in the boiler room. In an emergency, steam can be promptly shut off from these lines, leaving the steam supply entirely available for the fire pump. Strainers in steam lines to turbines are recommended.
- (b) The steam throttle at the pump should close against the steam pressure. It should preferably be of the globe pattern with a solid disc. If, however, the valve used has a removable composition ring, the disc should be of bronze and the ring made of sufficiently hard and durable material, and so held in place in the disc as to satisfactorily meet severe service conditions. Gate valves are undesirable for this service because they cannot so readily be made leaktight, as is possible with the globe type of valve. The steam piping should be so arranged and trapped that the pipes can be kept free of condensed steam.
- (c) In general, a pressure reducing valve should not be placed in the steam pipe supplying the fire pump. There is no difficulty in designing turbines for modern high-pressure steam, and this gives the simplest and most dependable unit. A pressure-reducing valve introduces a possible obstruction in the steam line in case it becomes deranged. In most cases the turbines may be protected by making the safety valve required by 10-2.1.2 of such size that the pressure in the casing will not exceed 25 psi (1.7 bars). This valve should be piped outside of the pump room and, if possible, to some point where the discharge could be seen by the pump attendant. Where a pressure-reducing valve is used, the following points should be carefully considered:

## 1. Pressure-Reducing Valve.

a. The pressure-reducing valve should not contain

a stuffing box or a piston working in a cylinder.

b. The pressure-reducing valve should be provided with a bypass containing a globe valve to be opened in case of an emergency. The bypass and stop valves should be one pipe size smaller than the reducing valve, and they should be located so as to be readily accessible. This bypass should be arranged to prevent the accumulation of condensate above the reducing valve.

- c. The pressure-reducing valve should be smaller than the steam pipe required by the specifications for the
- turbine.

2. Exhaust Pipe. The exhaust pipe should run direct to the atmosphere and should not contain valves of any type. It should not be connected with any condenser, heater, or

other system of exhaust piping.

3. Emergency Boiler Feed. A convenient method of ensuring a supply of steam for the fire pump unit, in case the usual boiler feed fails, is to provide an emergency connection from the discharge of the fire pump. This connection should have a controlling valve at the fire pump and also, if desired, an additional valve located in the boiler room. A check valve also should be located in this connection, preferably in the boiler room. This emergency connection should be about 2 in. (51 mm) in diameter.

This method should not be used when there is any danger of contaminating a potable water supply. In situations where the fire pump is handling salt or brackish water, it may also be undesirable to make this emergency boiler-feed connection. In such situations, an effort should be made to secure some other secondary boiler-feed supply that will always be available.

A-11-2.2 In addition, representatives of the installing contractor and owner should be present.

#### A-11-2.6 Fire Pump Operation.

- (a) Motor-Driven Pump. To start a motor driven pump, the following steps should be taken in the order given below:
  - 1. See that pump is completely primed.
  - 2. Close isolating switch and then close circuit breaker.
- 3. Automatic controller will start pump if system demand is not satisfied (pressure low, deluge tripped, etc.).
- 4. For manual operation, activate switch or pushbutton, or manual start handle.

NOTE: Circuit breaker tripping mechanism should be so set that it will not operate when current in circuit is excessively large.

- (b) Steam-Driven Pump. A steam turbine driving a fire pump should always be kept warmed up to permit instant operation at full rated speed. The automatic starting of the turbine should not be dependent on any manual valve operation or period of low-speed operation. If the pop safety valve on the casing blows, steam should be shut off and the exhaust piping examined for a possible closed valve or an obstructed portion of piping. Steam turbines are provided with governors to maintain speed at a predetermined point, with some adjustment for higher or lower speeds. Desired speeds below this range may be obtained by throttling the main throttle valve.
- (c) Diesel-Engine-Driven Pump. To start a diesel-engine-driven pump, the operator should be familiar beforehand with the operation of this type of equipment. The instruction books issued by the engine and control manufacturer should be studied to this end.

The storage batteries should always be maintained in good order to ensure prompt satisfactory operation of this equipment. Check electrolyte level and specific gravity, inspect cable conditions, corrosion, etc.

- (d) Fire Pump Settings. The fire pump system, when started by pressure drop, should be arranged as follows:
- 1. The jockey pump stop point should equal the pump churn pressure plus the minimum static supply pressure.
- 2. The jockey pump start point should be at least 10 psi less than the jockey pump stop point.
- 3. The fire pump start point should be 5 psi less than the jockey pump start point. Use 10 psi increments for each additional pump.
- 4. Where minimum run times are provided, the pump will continue to operate after attaining these pressures. The final pressures should not exceed the pressure rating of the system.
- 5. Where the operating differential of pressure switches does not permit these settings, the settings should be as close as equipment will permit. The settings should be established by pressures observed on test gauges.
  - 6. Example:

Pump: 1000 gpm, 100 psi pump with churn pressure of 115 psi. Suction Supply: 50 psi from city — minimum static. 60 psi from city — maximum static.

Jockey pump stop = 115 + 50 = 165 psi.

Jockey pump start = 165 - 10 = 155 psi.

Fire pump stop = 115 + 50 = 165 psi.

Fire pump start = 155 - 5 = 150 psi.

Fire pump maximum churn = 115 + 60 = 175 psi.

(For SI Units: 1 psi = 0.0689 bar.)

- 7. Where minimum run timers are provided, the pumps will continue to operate at churn pressure beyond the stop setting. The final pressures should not exceed the pressure rating of the system components.
- (e) Automatic Recorder. The performance of all fire pumps should be automatically indicated on a pressure recorder to provide a record of pump operation and assistance in fire loss investigation.
- A-11-2.6.1 Field Test Equipment. The test equipment should be furnished by either the authority having jurisdiction, or the installing contractor or the pump manufacturer, depending upon the prevailing arrangements made between the abovementioned parties.
- (a) Use with Test Valve Header. Fifty-foot (15-m) lengths,  $2\frac{1}{2}$ -in. (63.5-mm) lined hose, and Underwriters' play pipe nozzles as needed to flow required volume of water.

Exception: Where test meter is provided, these may not be needed.

- (b) Instrumentation. Test instruments should be of high quality, accurate, and in good repair.
  - 1. Clamp on volt/ammeter,
  - 2. Test gauges,
  - 3. Tachometer, and
  - 4. Pitot tube with gauge (for use with hose and nozzle).
- (c) Instrumentation Calibration. All test instrumentation should be calibrated by an approved testing and calibration facility within the 12 months prior to the test. Calibration documentation should be available for review by the authority having jurisdiction.

A majority of the test equipment used for acceptance and annual testing has not ever been calibrated. This equipment can have errors of 15 to 30 percent in readings. The use of uncalibrated test equipment may lead to inaccurate reported test results.

A-11-2.6.2 Where a hose valve header is used, it should be located where a limited [approximately 100 ft (30 m)] amount of hose is used to discharge water safely.

Where a flow test meter is used in a closed loop according to manufacturers' instructions, additional outlets such as hydrants, hose valves, etc., should be available to determine accuracy of metering device.

## A-11-2.6.3 Test Procedure.

- (a) Make a visual check of the unit. If hose and nozzles are used, see that they are securely tied down. See that the hose valves are closed. If a test meter is used, the valve on the discharge side of the meter should be closed.
  - (b) Start the pump.
- (c) Partially open one or two hose valves, or slightly open the meter discharge valve.
- (d) Check the general operation of the unit. Watch for vibration, leaks (oil or water), unusual noises, and general operation; adjust packing glands.
  - (e) Discharge of water:
- 1. Where test valve header is used, regulate the discharge by means of the hose valves and a selection of the nozzle tips. It will be noticed that the play pipe has a removable tip. This tip has a 1½-in. (28.6-mm) nozzle, and when the tip is removed, the play pipe has a 1¾-in. (44.4-mm) nozzle. Hose valves should be shut off before removing or putting on the 1½-in. (28.6-mm) tip.
- 2. Where test meter is used, regulate the discharge valve to achieve various flow readings.
- 3. Important test points are at 150 percent rated capacity, rated capacity, and shutoff.

Intermediate points may be taken if desired to help develop the performance curve.

- (f) Record the following data at each test point:
  - 1. Pump RPM.
  - 2. Suction pressure.
  - 3. Discharge pressure.
- 4. Number and size of hose nozzles, Pitot pressure for each nozzle, and total gpm (L/min). For test meter, record gpm (L/min).
  - 5. Amperes.
  - 6. Volts.

[See Figure A-11-2.6.3(f).]

- (g) Calculation of test results:
- 1. Rated Speed. Determine that pump is operating at rated RPM.
- 2. Capacity. For hose valve header, using a fire stream table, determine the gpm (L/min) for each nozzle at each Pitot reading. An example: 16 psi (1.1 bars) Pitot pressure with 1¾-in. (44.4-mm) nozzle indicates 364 gpm (1378 L/min). Add the gpm for each hose line to determine total volume.

For test meter, the total gpm (L/m) is read directly.

- 3. Total Head. For horizontal pumps this is the sum of:
- a. Pressure measured by discharge gauge at pump discharge flange,
- b. Velocity head difference, pump discharge, and pump suction,
- c. Gauge elevation corrections to pump centerline (plus or minus), and
- d. Pressure measured by suction gauge at pump suction flange; this value is negative when pressure is above zero.

For vertical pumps this is the sum of:

- a. Pressure measured by the discharge gauge at pump discharge flange,
  - b. Velocity head at the discharge,
  - c. Distance to the supply water level, and
- d. Discharge gauge elevation correction to centerline of discharge.
- 4. Electrical Input. Voltage and amperes are read directly from the volt/ammeter. This is compared to the motor name-plate full-load amperes. The only general calculation is to determine the maximum amperes allowed due to the motor service factor. In the case of 1.15 service factor, this is approximately 1.15 times motor amps, because changes in power factor and efficiency are not considered. If the maximum amps recorded on the test do not exceed this figure, the motor and pump will be judged satisfactory. It is most important to measure voltage and amperes accurately on each phase should the maximum amperes logged on the test exceed the calculated maximum amperes. This is important since a poor power supply with low voltage will cause a high ampere reading. This can be corrected only by improvement in the power supply; there is nothing that can be done to the motor or the pump.
- 5. Correction to Rated Speed. For purposes of plotting, the capacity, head, and power should be corrected from the test values at test speed to the rated speed of the pump. The corrections are made as follows:

Capacity:

$$Q_2 = \frac{N_2}{N_1} \times Q_1$$

Where

 $Q_1$  = Capacity at test speed in gpm (L/min)

 $Q_2$  = Capacity at rated speed in gpm (L/min)

 $N_1 = \text{Test speed in rpm}$ 

 $N_9$  = Rated speed in rpm

Head

$$H_2 = \left[\frac{N_2}{N_1}\right]^2 \times H_1$$

Where:

 $H_1$  = Head at test speed in ft (m)

 $H_2$  = Head at rated speed in ft (m)

Horsepower:

$$hp_2 = \left[\frac{N_2}{N_1}\right]^3 \times hp_1$$

Where:

 $hp_1 = horsepower (kW)$  at test speed

 $hp_2 = horsepower (kW)$  at rated speed

PUMP A	CC	EPTA	NCI	ΞT	ES	T C	DAT	Ά	Re	fer	to l	P &	ΡI	F(A	) – !	512	2.12	2 &	DS	3 –	· 7N	<u> </u>																
PROPERT	/ OF	•																		-								IN	IDEX	NO			C	DIST. OFFICE				
ADDRESS																												TE	STE	DΒ	Y		7	DATE				
CITY															S	TAT	E											PI	ACC	)			7	ODE	=			
SUBJECT															_							70	ONF	ERF	RED	WITH	•											
PUMP			SHA			אר	ΔI	ſ	٦,	/FRI	TICA	MANUFACTURER						1				1	APPROVED SH				SHC	HOP OR SERIAL NO.					T	MODEL OR TYPE				
			RAT					RATED HEAD-I									RATED RPM						SUCTION FROM				TANK				SIZE			TANK HEIGHT				
VER'	G/ W/	DIST. DISCH. GAUGE TO					TATIC FT				GHT- GLE AR		MANUFACTI MODEL OR									PE				HOP OR SERIAL NO							APPROVED YES NO					
	MAN			TUR	ER			F	Τ	AP	PPROV		J /ED SH			HOP OR SERIAL NO.				).	MODEL O			<u> </u>		H ROL					ATED	<u>—</u>						
DRIVER			_		ECT		:	RATED VOLT.				OPERA			ATING VOLT.			RATED F.L. AM				MPS	PS AMPS			AT 1	PI	PHASE			LES	SE	SERVICE FACTO			)R		
				DIE	SEI	L		] G/	GASOLINE ENGINE				GA:					TEAM URBINE			☐ PRES			SS. GOVERNOR			INDEF				PENDENT			TURBINE STEAM PRESS				
CONTR	SHC	NUF	ACT	TUR						ć	APPI Y	ROV ES				START MANUA			L	ps	osi			Р				si	JOCKEY F						– psi – psi			
SPEED RPM		PRES	HARGE SSURE PSI		SUCTION PRESSURE PSI		N RE	NET HEAD PSI			NO.		STREA! SIZE			MS PITOT PRESSURE			1			ONS PERCE RAT			ENT C	NT OF V				AMPS			STEAM PRE			•		
																																	$\perp$			$\perp$		
	_			Ļ							<u> </u>					1			_ _												$\perp$			$\perp$				
				L						<u> </u>					$\downarrow$			_ _			$\perp$												$\perp$					
	_			╀							↓_					$\downarrow$				1				_			4-			$\downarrow$			$\downarrow$			_		
			╀					-	,				+			+			+-	<u> </u>		+	+			-					+							
Readings marked (+) in suction column are heads above atmosphere, those marked (-) are lifts.  For vertical shaft pumps omit suction pressure and net head readings.																_	丄																					
											For	vertic	cal s	haft	pum	os o	mit s	uctio	on pr	essu	ire ai	nd n	et he	ad r	eadir	ngs.			_				_		_	180		
18	-	4		4	_	_	_	_									_	_	_			_		_	_		_	<u> </u>		L	ļ		4	$\exists$	$\Box$	160		
	60	+	$\vdash$	-			<del> </del>	-	<del> </del>	_	-	_		_				-		-					_	-	╣	╁	╁	-	-	Н	$\dashv$	$\dashv$	$\dashv$	160		
14	ה. ב			╛																														1		140		
•	_	+	$\vdash$	-		_	$\vdash$	_	_					+	<u> </u>	$\vdash$	$\vdash$	$\dashv$				<u> </u>		$\square$	-		4-	igdot	₩	$ \_ $	$\sqcup$	$\vdash \vdash$	$\dashv$	$\dashv$	$\dashv$	140		
12	0		+	7	$\dashv$	_	<del> </del>	╁╴	$\vdash$		$\vdash$	-	_	_			_	-		-		┢╌				-	+	╁╴	-	<del> </del>	┢	-	$\dashv$	$\dashv$	$\dashv$	120		
() 10	n	1																																$\Box$		100	ģ	
Pressure (Ib/in²)	<b>~</b>  -		$\vdash$	$\dashv$	-	_	┝	_	<del> </del>	_	H	_	_	_				_	_	_		-				_	- -	┼	┨—	_	-		$\dashv$	$\dashv$	긕		Amperes	
SSOUI 8	아			1		-	-	╁╴	┢		Н			_		_		-			Н	-	-			+	+	╁	$\vdash$	-	╁	$\vdash$	$\dashv$	十	ㅓ	80	Ą	
	0																																$\Box$	$\sqsupset$	$\Box$	60		
•	~  -	-	-	-				-	-									_	_	_		<u> </u>	_	<del> </del>	_			+	-		_	$\vdash$	$\dashv$	4	$\dashv$			
4	아	+	$\vdash$	┪	_		-	╁	-		_		_	_			-		_		Н					_	$\dagger$	╁	$\dagger$	<del> </del>	╁╴		$\dashv$	$\dashv$	$\dashv$	40	I	
2	20	1		$\Box$																							1		$\Box$			П	$\Box$	$\Box$		20		
_	}		-	4	$\dashv$		_	-	_		$\vdash$	$\vdash$	_	_	$\mid \rightarrow \mid$		_	-		_	$\vdash$	-		_	H		-	╁	┼	-	-	$\vdash$	$\dashv$	+	$\dashv$			
	0	1	0	20	0	3	30	4	0	5	0	6	0	7	'O F		iO cent		O ed o		DO acity		10	1:	20	130	) .	40	1:	L 50	11	60	17	<u></u> L	18	,0		
Plot	disc	harge p	ressu	e a	nd n	et h	ead	curv	es fo	r ho	rizon	tal si	haft (	pum									harge	e pre	ssur	e curv	e. For	elec	tric-d	river	pun	np, pl	ot ar	npere	e cui	ve al:	50.	

105 (9-77) ENGINEERING PRINTED IN USA

(Courtesy of Factory Mutual Research Corp.)

Figure A-11-2.6.3(f) Pump acceptance test data.

- 6. Conclusion. The final step in the test calculation is generally a plot of test points. A head capacity curve is plotted, and an ampere capacity curve is plotted. A study of these curves will show the performance picture of the pump as it was tested.
- A-11-2.7.1 All controller starts required for tests described in 11-2.6, 11-2.7, 11-2.8, and 11-2.10 should accrue respectively to this number of tests.

# Appendix B Possible Causes of Pump Troubles

This Appendix is not a part of the requirements of this NFPA document but is included for informational purposes only.

This appendix contains a partial guide for locating pump troubles and their possible causes. It also contains a partial list of suggested remedies. For other information on this subject, see Hydraulics Institute Standards for Centrifugal, Rotary and Reciprocating Pumps. (See Appendix C, Referenced Publications.)

The causes listed here are in addition to possible mechanical breakage that would be obvious on visual inspection. In case of trouble it is suggested that those troubles that can be checked easily should be corrected first or eliminated as possibilities.

- B-1 Air Drawn into Suction Connection Through Leak(s). Air drawn into suction line through leaks causes a pump to lose suction or fail to maintain its discharge pressure. Uncover suction pipe and locate and repair leak(s).
- **B-2 Suction Connection Obstructed.** Examine suction intake, screen, and suction pipe and remove obstruction. Repair or provide screens to prevent recurrence. (See 2-9.8.)
- **B-3** Air Pocket in Suction Pipe. Air pockets cause a reduction in delivery and pressure similar to an obstructed pipe. Uncover suction pipe and rearrange to eliminate pocket. (See 2-9.6.)
- **B-4** Well Collapsed or Serious Misalignment. Consult a reliable well drilling company and the pump manufacturer regarding recommended repairs.
- B-5 Stuffing Box too Tight or Packing Improperly Installed, Worn, Defective, too Tight, or Incorrect Type. Loosen gland swing bolts and remove stuffing box gland halves. Replace packing.
- **B-6 Water Seal or Pipe to Seal Obstructed.** Loosen gland swing bolt and remove stuffing box gland halves along with the water-seal ring and packing. Clean the water passage to and in the water-seal ring. Replace water-seal ring, packing gland, and packing in accordance with manufacturer's instructions.
- B-7 Air Leak into Pump Through Stuffing Boxes. Same as possible cause B-6.
- **B-8 Impeller Obstructed.** Does not show on any one instrument, but pressures fall off rapidly when an attempt is made to draw a large amount of water.

For horizontal split-case pumps: Remove upper case of pump and remove obstruction from impeller. Repair or provide screens on suction intake to prevent recurrence.

For vertical shaft turbine-type pumps: Lift out column pipe (see Figures A-4-2.2.1 and A-4-2.2.2) and pump bowls from wet pit or well and disassemble pump bowl to remove obstruction from impeller.

For close-coupled, vertical in-line pumps: Lift motor on top pull-out design and remove obstruction from impeller.

- **B-9 Wearing Rings Worn.** Remove upper case and insert feeler gauge between case wearing ring and impeller wearing ring. Clearance when new is 0.0075 in. (0.19 mm). Clearances of more than 0.015 in. (0.38 mm) are excessive.
- **B-10 Impeller Damaged.** Make minor repairs or return to manufacturer for replacement. If defect is not too serious, order new impeller and use damaged one until replacement arrives.
- **B-11 Wrong Diameter Impeller.** Replace with impeller of proper diameter.
- **B-12** Actual Met Head Lower than Rated. Check impeller diameter and number and pump model number to make sure correct head curve is being used.
- B-13 Casing Gasket Defective Permitting Internal Leakage (Single-Stage and Multi-Stage Pumps). Replace defective gasket. Check manufacturer's drawing to see if gasket is required.
- **B-14** Pressure Gauge is on Top of Pump Casing. Place gauges in correct location. (See Figure A-3-3.1.)
- B-15 Incorrect Impeller Adjustment (Vertical Shaft Turbine-Type Pump Only). Adjust impellers according to manufacturer's instructions.

#### B-16 Impellers locked.

For vertical shaft turbine-type pumps: Raise and lower impellers by the top shaft adjusting nut. If this is not successful, follow the manufacturer's instructions.

For horizontal split-case pumps: Remove upper case and locate and eliminate obstruction.

- **B-17 Pump is Frozen.** Provide heat in the pump room. Disassemble pump and remove ice as necessary. Examine parts carefully for damage.
- B-18 Pump Shaft or Shaft Sleeve Scored, Bent, or Worn. Replace shaft or shaft sleeve.
- **B-19 Pump Not Primed.** If a pump is operated without water in its casing, the wearing rings are likely to seize. The first warning is a change in pitch of the sound of the driver. Shut down the pump.

For vertical shaft turbine-type pumps: Check water level to determine if pump bowls have proper submergence.

- B-20 Seal Ring Improperly Located in Stuffing Box, Preventing Water from Entering Space to Form Seal. Loosen gland swing bolt and remove stuffing box gland halves along with the water-seal ring and packing. Replace, putting seal ring in proper location.
- B-21 Excess Bearing Friction Due to Lack of Lubrication, Wear, Dirt, Rusting, Failure, or Improper Installation. Remove bearings and clean, lubricate, or replace as necessary.
- **B-22** Rotating Element Binds Against Stationary Element. Check clearances and lubrication and replace or repair the defective part.
- **B-23 Pump and Driver Misaligned.** Shaft running off center because of worn bearings or misalignment. Align pump and driver according to manufacturer's instructions. Replace bearings according to manufacturer's instructions. (See Section 3-5.)
- **B-24 Foundation Not Rigid.** Tighten foundation bolts or replace foundation if necessary. (See Section 3-4.)